

# Influence of laser pulse on plane waves propagating in a thermoelastic medium with micro-temperature under the DPL model

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**Abstract.** In this paper, estimation is made to investigate the influence of thermal loading due to laser pulse on elastic waves. The material through which the waves are propagating is homogeneous and isotropic in nature. Heat conduction through the media is analyzed by the model proposed by dual-phase-lag theory (DPL). The governing non-dimensional equations are solved by using the approximated harmonic solution. The expression for the field variables is obtained generally and represented graphically for a particular medium.

**Keywords:** thermoelastic wave, thermal loading, micro-temperature, DPL model, harmonic solution.

## 1. Introduction

Very rapid thermal processes under the action of an ultra-short laser pulse are interesting from the standpoint of thermoelasticity because they require deformation fields and an analysis of the coupled temperature. This means that the laser pulse energy absorption results in a localized temperature increase, which causes thermal expansion and generates rapid movements in the structure elements, thus causing the rise in vibrations. These effects make materials susceptible to the diffusion of heat by conduction.

The ultra-short lasers are those with the pulse duration ranging from nanoseconds to femtoseconds. The high intensity, energy flux, and ultra-short duration laser beam have studied situations where very large thermal gradients or an ultra-high heating rate may exist on the boundaries, this in the case of ultra-short-pulsed laser heating [1, 2]. The microscopic two-step models that are parabolic and hyperbolic are useful for modifying the material as thin films. When a metal film is heated by a laser pulse, a thermoelastic wave is generated due to thermal expansion near the surface. The stress wave induced by pico and femtosecond laser pulses in a semi infinite metal by expressing the laser pulse energy as a Fourier series was studied by Wang and Xu [3]. The effect of rotation on a fiber-reinforced on the generalized magneto-thermoelasticity subject to thermal loading due to the laser pulse was studied by [4]. The effect of Thomson and initial stress in a thermo-porous elastic solid under G-N electromagnetic theory was discussed by [5]. The effect of the laser pulse on transient waves in a nonlocal thermoelastic medium under G-N theory was explained by [6].

A unified filed approach for heat conduction from macro to macro scales was investigated by [7]. A simplest thermoelasticity theory with microtemperatures that takes under consideration many new variables was presented by [8]. Quintanilla and Rache [9] pointed out a note on stability in dual-phase-lag heat conduction. The propagation of harmonic plane waves with assigned frequency by employing the thermoelasticity theory with DPL model was presented by [10]. The problems related with DPL model heat conduction model were considered by [11-13] and many others.

The heat conduction in materials with micro-temperatures was discussed by [14]. He has

examined his theoretical results, with excellent agreement, by comparing them with the experimental data. The effect of initial stress and hall current on a magneto-thermoelastic porous medium with micro-temperatures was presented by [15]. The theory of heat conduction in micromorphic continua with micro-temperatures was developed by [16]. Some, boundary value problems of the linear theory of thermoelasticity with micro-temperatures for different structures with applications are constructed by many investigators. The propagation of Rayleigh waves in a microstretch thermoelastic half-space with microtemperatures in context of L-S [17] theory of thermoelasticity was presented by [18]. The effect of initial stress on a porous thermoelastic medium with micro-temperatures was discussed by [19]. The magneto-thermoelastic solid with micro-temperatures and voids was studied by [20]. The relaxation effects of the volume properties of electrically conducting viscoelastic material were explained by [21]. The effect of Thomson and thermal loading due to laser pulse in a magneto-thermoelastic porous medium with energy dissipation was studied by [22]. Othman and Abouelregal [23] explained the effect of pulsed laser radiation on a thermo-visco-elastic semi-infinite solid under two-temperature theory. The effect of laser pulse and gravity field on thermoelastic medium under Green-Naghdi theory was studied by [24].

In this chapter we have considered a special type of heat source responsible of wave generation in thermoelastic medium. We have designed a thermoelastic medium model and the material is a homogeneous isotropic heated by laser pulse. To analyze the problem and get the numerical solutions for the temperature distribution, displacement function, stress components, normal mode analysis method is used. Finally, the theoretical results obtained are represented graphically for particular medium.

## 2. Problem formulation and basic equations

We have considering a generalized homogeneous isotropic thermoelastic medium with micro temperature and without any body-force while laser pulse is considered as the heat source. The rectangular Cartesian coordinates  $(x, y, z)$  are used to represent the geometry of the half-space medium  $z \geq 0$ , with  $z$  axis vertically into the medium. All the quantities in the problem will be in form of coordinates  $x$  and  $z$  and time  $t$  as variable function.

The set of constitutive equations are:

$$\begin{cases} \sigma_{ij} = \lambda \delta_{ij} e_{kk} + 2\mu e_{ij} - \beta \theta \delta_{ij}, \\ q_{ij} = -k_4 w_{r,r} \delta_{ij} - k_5 w_{i,j} - k_6 w_{j,i}, \\ Q_i = (K - k_3) \theta_{,i} + (k_1 - k_2) w_{i}, \\ q_i = K \theta_{,i} + k_1 w_i, \end{cases} \quad (1)$$

where  $Q$  is heat input on laser pulse effects on heat equation and is representing, heat input in form of beam or laser-pulse [1]. We suppose that all functions are differentiable and continuous in the defined domain:

$$Q = \frac{I_0 \gamma^* t}{2\pi r^2 t_0^2} \exp\left(-\frac{x^2}{r^2} - \frac{t}{t_0}\right) + \gamma^* y, \quad (2)$$

where  $I_0$  is heat absorbed  $t_0$  is pulse rise,  $r$  is radius of beam,  $\gamma^*$  is depth of absorbing heat energy and with  $t$  time variable. The system of governing equations can be represented as:

$$\mu \nabla^2 \mathbf{u} + (\lambda + \mu) \nabla(\nabla \cdot \mathbf{u}) - \beta \nabla \theta = \rho \frac{\partial^2 \mathbf{u}}{\partial t^2}, \quad (3)$$

$$k_6 \nabla^2 \mathbf{w} + (k_4 + k_5) \nabla(\nabla \cdot \mathbf{w}) - k_3 \nabla \theta - k_2 \mathbf{w} - b \frac{\partial \mathbf{w}}{\partial t} = 0, \quad (4)$$

$$\left(1 + \tau_T \frac{\partial}{\partial t}\right) \theta_{,ii} + \frac{k_1}{K} (\nabla \cdot \mathbf{w}) = \left(1 + \tau_q \frac{\partial}{\partial t}\right) \left(\frac{\rho c_e}{K} \frac{\partial \theta}{\partial t} + \frac{\beta \theta_0}{K} \frac{\partial e_{kk}}{\partial t} - \frac{\rho Q}{K}\right). \quad (5)$$

Introducing the following variables to dimensionless the governing system of equation:

$$\begin{aligned} x'_i &= \frac{x_i}{l_0}, \quad t' = \frac{c_1 t}{l_0}, \quad u'_i = \frac{u_i}{l_0}, \quad \theta' = \frac{\theta}{\theta_0}, \quad w'_i = w_i l_0, \\ \tau'_T &= \frac{c_1 \tau_T}{l_0}, \quad \tau'_q = \frac{c_1 \tau_q}{l_0}, \quad \nabla'^2 = \frac{1}{l_0^2} \nabla'^2, \quad Q' = \frac{l_0 Q}{c_1 \theta_0 C_e}. \end{aligned} \quad (6)$$

where,  $l_0$  is standard length and  $c_1$  is the standard velocity given by  $c_1 = \sqrt{(\lambda + 2\mu/\rho)}$ . After non dimensional the governing equations can be represented as, (primes are dropped for simplicity):

$$\alpha_0 \nabla^2 \mathbf{u} + \alpha_1 \nabla (\nabla \cdot \mathbf{u}) - H \nabla \theta = \frac{\partial^2 \mathbf{u}}{\partial t^2}, \quad (7)$$

$$\beta_0 \nabla^2 \mathbf{w} + \beta_1 \nabla (\nabla \cdot \mathbf{w}) - \beta_2 \nabla \theta - \beta_3 \mathbf{w} - \beta_4 \frac{\partial \mathbf{w}}{\partial t} = 0, \quad (8)$$

$$\alpha_2 \left(1 + \tau_T \frac{\partial}{\partial t}\right) \theta_{,ii} + \alpha_3 (\nabla \cdot \mathbf{w}) = \left(1 + \tau_q \frac{\partial}{\partial t}\right) \left(\frac{\partial \theta}{\partial t} + \alpha_4 \frac{\partial e_{kk}}{\partial t} - Q\right), \quad (9)$$

where:

$$\begin{aligned} \alpha_0 &= \frac{\mu}{\rho c_1^2}, \quad \alpha_1 = \frac{(\lambda + \mu)}{\rho c_1^2}, \quad \alpha_2 = \frac{K}{l_0 \rho c_e c_1}, \quad \alpha_3 = \frac{k_1}{l_0 \rho \theta_0 c_e c_1}, \quad \alpha_4 = \frac{\beta}{\rho c_e}, \\ H &= \frac{\beta' \theta_0}{\rho c_1^2}, \quad \beta_0 = \frac{k_6}{l_0^3}, \quad \beta_1 = \frac{(k_4 + k_5)}{l_0^3}, \quad \beta_2 = \frac{k_3}{l_0}, \quad \beta_3 = \frac{k_2}{l_0}, \quad \beta_4 = \frac{b}{l_0^2}. \end{aligned} \quad (10)$$

Displacement and micro-temperature functions could be converted in terms of potential function by following expression [18]:

$$u_1 = \left(\frac{\partial R}{\partial x} + \frac{\partial \psi}{\partial z}\right), \quad u_3 = \left(\frac{\partial R}{\partial z} - \frac{\partial \psi}{\partial x}\right), \quad w = \nabla v, \quad (11)$$

where,  $R$  and  $v$  are scalar potentials functions, and vector potential is representing by  $\psi$ . After some algebraic calculations the above equations become:

$$(\alpha_0 + \alpha_1) \nabla^2 R - H \phi = \frac{\partial^2 R}{\partial t^2}, \quad (12)$$

$$\alpha_0 \nabla^2 \psi = \frac{\partial^2 \psi}{\partial t^2}, \quad (13)$$

$$\sigma \nabla^2 v - \beta_2 \phi - \beta_3 v - \beta_4 \frac{\partial v}{\partial t} = 0, \quad (14)$$

$$\alpha_2 \left(1 + \tau_T \frac{\partial}{\partial t}\right) \nabla^2 \theta + \alpha_3 \nabla^2 v - \left(1 + \tau_q \frac{\partial}{\partial t}\right) \left(\frac{\partial \theta}{\partial t} + \alpha_4 \nabla^2 \frac{\partial R}{\partial t} - Q\right) = 0. \quad (15)$$

## 2.1. Harmonic solution of the problem

Now let us consider that each field variable is propagating through the medium in terms of harmonic waves as:

$$\{R, \phi, v, \psi\}(x, z, t) = \{R^*, \phi^*, v^*, \psi^*\}(z) \exp(\omega t + iax), \quad (16)$$

where  $\omega$  is the angular frequency  $i = \sqrt{-1}$ ,  $a$  is the wave number in the  $z$ -direction and  $R^*$ ,  $\phi^*$ ,  $v^*$ ,  $\psi^*$  are the amplitudes in the field quantity. By using Eq. (15) in Eqs. (11)-(14) can be represented as:

$$(\alpha D^2 + A_1)R^* - H\theta^* = 0, \quad (17)$$

$$(\alpha_0 D^2 + A_3)\psi^* = 0, \quad (18)$$

$$(\sigma D^2 - A_7)v^* - \beta_2\theta^* = 0, \quad (19)$$

$$(\alpha_2 D^2 \pi_1 + A_5)\theta^* + \alpha_3(D^2 - a^2)v^* + (-\alpha_4 D^2 \pi_2 + A_6)R^* \\ = \left[ -tQ_0 - \tau_q Q_0 \left( 1 - \frac{t}{t_0} \right) \exp(-\omega t - iax) \right], \quad (20)$$

where:

$$A_1 = -\alpha a^2 - w^2, \quad A_3 = -\alpha_0 a^2 - w^2, \\ \pi_1 = (1 + \tau_T \omega), \quad \pi_2 = (\omega + \tau_q \omega^2), \quad Q_0 = \frac{I_0 \gamma^*}{2\pi r^2 t_0^2} \exp\left(-\frac{x^2}{r^2} - \frac{t}{t_0} + \gamma^* z\right). \quad (21)$$

For nontrivial solution the determinant of the above system of equations need to be zero, it implies:

$$[D^6 - A D^4 + B D^2 - C] \{\theta^*, v^*, R^*\}(z) = (L_1, L_2, L_3) f^*(x, t) \exp(\gamma^* z), \quad (22)$$

where:

$$A = -\frac{A_1}{g_6} - g_8 + g_9 - g_{10} + g_{21}, \quad B = g_{11} - g_{12} - g_{13} - g_{14} + g_{15} + g_{16} + g_{17}, \\ C = g_{18} + g_{19} + g_{20}, \quad L_1 = \frac{\gamma^{*4}}{g_2} + \frac{A_1 \gamma^{*2}}{g_2 g_6} + \frac{A_7 \gamma^{*2}}{g_2 g_3} - \frac{A_1 A_7}{g_1}, \\ L_2 = \frac{\beta_2 \gamma^{*2}}{g_2 g_3} + \frac{A_1 \beta_2}{g_1}, \quad L_3 = \frac{H \gamma^{*2}}{g_2 g_6} + \frac{H A_7}{g_1}, \\ f^*(x, t) = \frac{I_0 \gamma^*}{2\pi r^2 t_0^2} \exp\left(-\frac{x^2}{r^2} - \frac{t}{t_0}\right) \left[ -t - \tau_q \exp(\omega t + iax) + \frac{t}{t_0} \exp(\omega t + iax) \right], \\ g_1 = \alpha \alpha_2 \pi_1 \sigma, \quad g_2 = \alpha_2 \pi_1, \quad g_3 = \sigma, \quad g_4 = \alpha_3 \beta_2, \quad g_5 = \alpha_4 \pi_2 \beta, \\ g_6 = \alpha, \quad g_7 = \alpha \alpha_2 \pi_1, \quad g_8 = \frac{A_5}{g_2}, \quad g_9 = \frac{A_7}{g_3}, \quad g_{10} = \frac{g_4}{g_2 g_3}, \\ g_{11} = \frac{A_1 g_8}{g_6}, \quad g_{12} = \frac{A_1 g_9}{g_6}, \quad g_{13} = \frac{A_5 A_7}{g_7}, \quad g_{14} = g_{10} a^2, \quad g_{15} = g_{10} A_1, \\ g_{16} = \frac{A_6 \beta}{g_7}, \quad g_{17} = \frac{g_5 A_7}{g_1}, \quad g_{18} = \frac{A_1 g_7 g_{13}}{g_1}, \quad g_{19} = \frac{g_{14}}{g_1}, \\ g_{20} = \frac{A_6 g_{16}}{g_1}, \quad g_{21} = \frac{g_5}{g_1}, \quad D = \frac{d}{dz}.$$

Now Eq. (22) can be factored as:

$$(D^2 - k_1^2)(D^2 - k_2^2)(D^2 - k_3^2)\theta^*(z) = L_1 f^*(x, t) \exp(\gamma^* z). \quad (23)$$

Whereas, the roots of characteristic equation are  $k_i^2$ ,  $i = 1, 2, 3$ . The general solution of the problem is given by:

$$\theta(x, z, t) = \sum_{n=1}^3 M_n \exp(-k_n z + \omega t + iax) + N_1 L_1 f^*(x, t) \exp(\gamma^* z), \quad (24)$$

$$\psi(x, z, t) = M_4 \exp(-k_4 z + \omega t + iax), \quad (25)$$

$$v(x, z, t) = \sum_{n=1}^3 H_{1n} M_n \exp(-k_n z + \omega t + iax) + N_1 L_2 f^*(x, t) \exp(\gamma^* z), \quad (26)$$

$$R(x, z, t) = \sum_{n=1}^3 H_{2n} M_n \exp(-k_n z + \omega t + iax) + N_1 L_3 f^*(x, t) \exp(\gamma^* z), \quad (27)$$

where  $k_4^2 = -A_3/\alpha_0$  are roots of the characteristic Eq. (23) and  $M_n$  are some coefficients to be find:

$$N_1 = \frac{1}{\gamma^{*6} - A\gamma^{*4} + B\gamma^{*2} - C}, \quad H_{1n} = \frac{\beta_2}{(\sigma k_n^2 - A_7)}, \quad H_{2n} = \frac{H}{(\sigma k_n^2 + A_1)}, \quad (28)$$

$$f^*(x, t) = \frac{I_0 \gamma^*}{2\pi r^2 t_0^2} \exp\left(-\frac{x^2}{r^2} - \frac{t}{t_0}\right) \left[-t - \tau_q + \frac{t}{t_0}\right].$$

Using the relation of potential functions we get:

$$u_1 = \left[ \sum_{n=1}^3 ia M_n H_{2n} \exp(-k_n z) - k_4 M_4 \exp(-k_4 z) \right] \exp(iax + \omega t) - \frac{2x}{r^2} N_1 L_3 f^*(x, t) \exp(\gamma^* z), \quad (29)$$

$$u_3 = \left[ \sum_{n=1}^3 (-k_n) M_n H_{2n} \exp(-k_n z) - ia M_4 \exp(-k_4 z) \right] \exp(iax + \omega t) + \gamma^* N_1 L_3 f^*(x, t) \exp(\gamma^* z), \quad (30)$$

$$w_1 = \sum_{n=1}^3 ia H_{1n} M_n \exp(-k_n z + \omega t + iax) - \left(\frac{2x}{r^2}\right) N_1 L_2 f^*(x, t) \exp(\gamma^* z), \quad (31)$$

$$w_3 = \sum_{n=1}^3 -k_n H_{1n} M_n \exp(-k_n z + \omega t + iax) + (\gamma^*) N_1 L_2 f^*(x, t) \exp(\gamma^* z). \quad (32)$$

The components of stress are:

$$\sigma_{zz} = \left[ \sum_{n=1}^3 M_n H_{5n} \exp(-k_n z) + N_7 M_4 \exp(-k_4 z) \right] \exp(iax + \omega t) + N_8 f^*(x, t) \exp(\gamma^* z), \quad (33)$$

$$\sigma_{xz} = \left[ \sum_{n=1}^3 M_n H_{3n} \exp(-k_n z) + N_2 M_4 \exp(-k_4 z) \right] \exp(iax + \omega t) + N_3 f^*(x, t) \exp(\gamma^* z), \quad (34)$$

where:

$$H_{3n} = -2ia\alpha_0 k_n H_{2n}, \quad N_2 = \alpha_0 (k_4^2 + a^2), \quad N_3 = \frac{-4x\alpha_0 \gamma^*}{r^2} L_3 N_1, \quad (35)$$

$$H_{5n} = [\alpha(k_n^2 - a^2) - 2ia\mu k_n] H_{2n} - \beta\theta_0,$$

$$N_7 = 2\mu a^2, \quad N_8 = N_1 \left[ \frac{-2\lambda L_3}{r^2} + \frac{4\lambda x^2}{r^4} L_3 + \lambda L_3 \gamma^{*2} - \frac{4x\mu \gamma^*}{r^2} L_3 - \beta\theta_0 \right].$$

## 2.2. Boundary conditions

The boundary conditions assumed at the surface  $z = 0$  to find the remaining unknown constants used in above exponential solution of the problem are,

1) Time dependent periodic force with magnitude  $f(x, 0, t)$  is assumed to be acting normally on the medium, while tangentially the medium is considered as isolated from the surrounding:

$$\sigma_{zz}(x, 0, t) = f_0 \exp(\omega t + ia x), \quad (36)$$

$$\sigma_{xz}(x, 0, t) = 0, \quad (37)$$

where  $f_0$  is an arbitrary constant function.

2) From condition on thermal boundary condition, the surface of half space is at some fixed temperature:

$$\theta(x, 0, t) = \theta_0 \exp(\omega t + ia x). \quad (38)$$

3) Normal component of heat flux moment vector is zero:

$$q_{zz} = 0. \quad (39)$$

By applying the above obtained solutions in boundary conditions, we get:

$$\sum_{n=1}^3 M_n H_{5n} + N_7 M_4 = f_0, \quad (40)$$

$$\sum_{n=1}^3 M_n H_{3n} + N_2 M_4 = 0, \quad (41)$$

$$\sum_{n=1}^3 M_n = \theta_0, \quad (42)$$

$$\sum_{n=1}^3 \pi_{7n} H_{1n} M_n = 0, \quad (43)$$

where,  $\pi_{7n} = [k_4 a^2 + (k_4 + k_5 + k_6) k_n^3]$ .

To find the values of  $M_n$ ,  $n = 1, 2, 3$ , and  $M_4$  we will apply matrix inversion method on system of equations:

$$\begin{bmatrix} M_1 \\ M_2 \\ M_3 \\ M_4 \end{bmatrix} = \begin{bmatrix} H_{51} & H_{52} & H_{53} & N_7 \\ H_{31} & H_{32} & H_{33} & N_2 \\ 1 & 1 & 1 & 0 \\ \pi_{71} H_{11} & \pi_{72} H_{12} & \pi_{73} H_{13} & 0 \end{bmatrix}^{-1} \begin{bmatrix} f_0 \\ 0 \\ \theta_0 \\ 0 \end{bmatrix}. \quad (44)$$

Hence, we obtain the solution of each field variable.

### 2.3. Numerical results and discussion

The evaluated theoretical results are computed numerically by using the relevant parameters for the case of magnesium crystal. The relevant physical values of elastic constants and micro-temperatures as [20]:  $\rho = 1.74 \times 10^3 \text{ kgm}^{-3}$ ,  $\lambda = 9.4 \times 10^{10} \text{ Nm}^{-2}$ ,  $\mu = 4.0 \times 10^{10} \text{ Nm}^{-2}$ ,  $\beta = 7.779 \times 10^{-8} \text{ N}$ ,  $C_e = 1.04 \times 10^3 \text{ NmKg}^{-1} \text{ K}^{-1}$ ,  $\theta_0 = 0.298$ ,  $b = 0.15 \times 10^9 \text{ N}$ .

The micro-temperature parameters are,  $k_1 = 0.0035 \text{ Ns}^{-1}$ ,  $k_2 = 0.045 \text{ Ns}^{-1}$ ,  $k_3 = 0.055 \text{ NK}^{-1} \text{ s}^{-1}$ ,  $k_4 = 0.064 \text{ Ns}^{-1} \text{ m}^2$ ,  $k_5 = 0.075 \text{ Ns}^{-1} \text{ m}^2$ ,  $k_6 = 0.096 \text{ Ns}^{-1} \text{ m}^2$ .

The computations of figure (a) are carried out for different values of the time parameter  $t$ , to see the variations because of different time for laser pulse while  $t_\tau = 0.015 \text{ sec}$  and  $t_q = 0.02 \text{ sec}$ . In the figures (part-b) is representing the variations because of  $t_\tau$  and  $t_q$  and  $t = 0.1 \text{ sec}$ . Graphical representation is made for low values for wave number  $a = 0.001 \text{ cycle/second}$  the plane  $x = 1$ . The non-dimensional field variables as, the temperature, displacement components, micro-temperature components, normal stress and tangential stress distribution functions are

represented graphically for different values of time parameter  $t$ .

Fig. 1 depicts the behavior of heat propagating through the medium under different conditions of times. From part-a, it can be analyzed that the maximum value of the amplitude increases as the value of time  $t$  increases. Part-b indicates the absolute value of the temperature gradient and heat fluxes are directly proportional to all the three-time lags. The curves converge to zero as the vertical distance from the surface increases indicating the waves to be surface waves in nature.

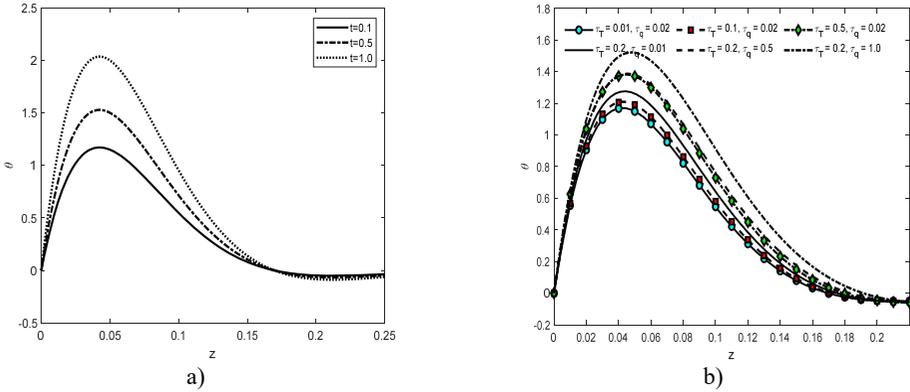


Fig. 1.  $\theta$  against  $z$  for different time

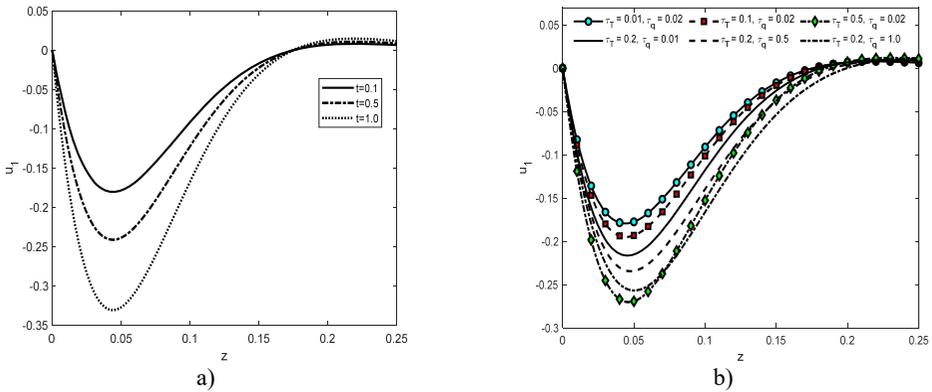


Fig. 2.  $u_1$  against depth for different values of time

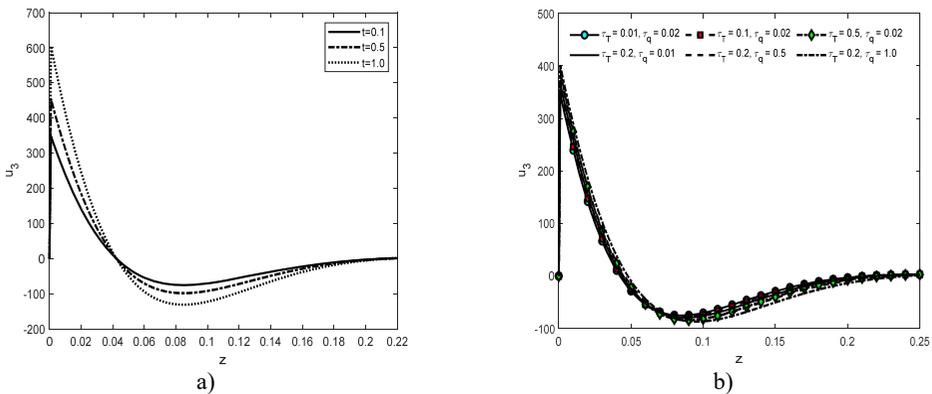


Fig. 3.  $u_3$  against depth for different values of  $t$

Fig. 2 represents the behavior of horizontal component of displacement against vertical component of distance. It can be analyzed that the absolute value of the curves increases by

increasing the time parameter involved in the model of the system. Similarly, phase lags are directly proportional to the absolute value of the amplitude of wave propagating through the medium. Graphical analysis of vertical component of displacement is represented in Fig. 3.

The curves for vertical components of displacement are responding to time parameter same as  $u_1$  and the cases the curves for  $t = 0.1$  converge to zero first. Phase lags  $\tau_T$  and  $\tau_q$  are having decreasing effect for some initial values of vertical distance but for depth  $> 0.075$  the behavior reversed. Convergence of curve toward zero reduces as the times increases. Micro-temperature components against vertical component of distance are shown in Fig. 4 and Fig. 5. Time parameter is having increasing effect on absolute values of the amplitude of waves generated because of non-dimensional components of micro-temperature. It can be analyzed that the convergence rate of the curve is inversely proportional to the times. Greater the value of time lag  $\tau_q$  higher the amplitude of the curve, it also reduces the convergence rate of the particle toward equilibrium. Similarly, the influence of  $\tau_T$  is directly proportional to the amplitude of waves propagating through the medium. The curves in context of  $\tau_q = 0.02$ ,  $\tau_T = 0.01$  damped to zero faster than all the other conditions. Variation in Normal component of stress distribution function against time parameter is graphically represented in Fig. 6. Over all curves are having increasing effect of stress wave. The amplitude increases for  $0 \leq z \leq 0.042$  and decreasing for the other values of vertical component of distance. The curves for  $t = 0.01$  converge to zero earlier than the curves for higher value of time parameter.

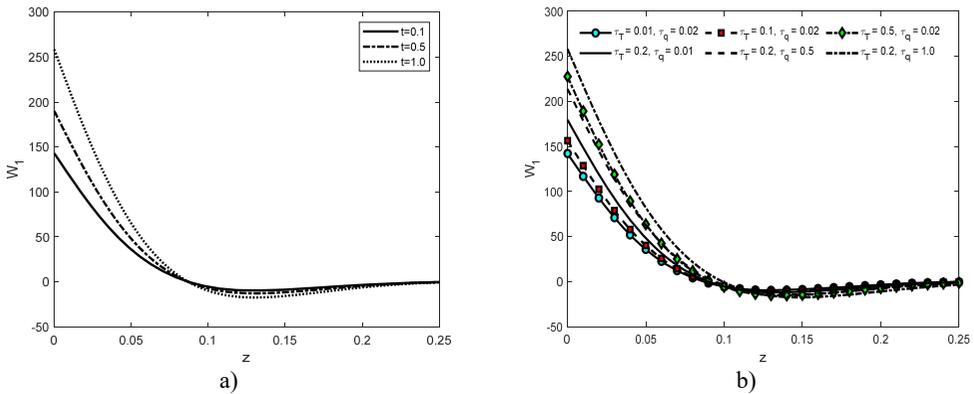


Fig. 4. Micro-temperature 1st component against different values of time

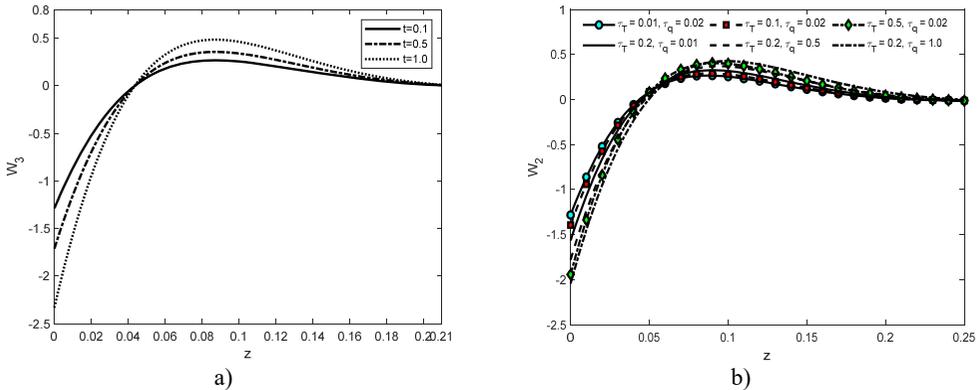
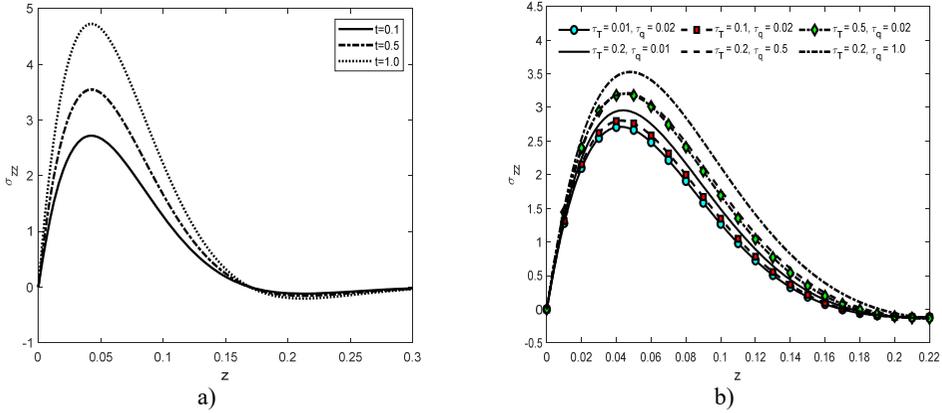


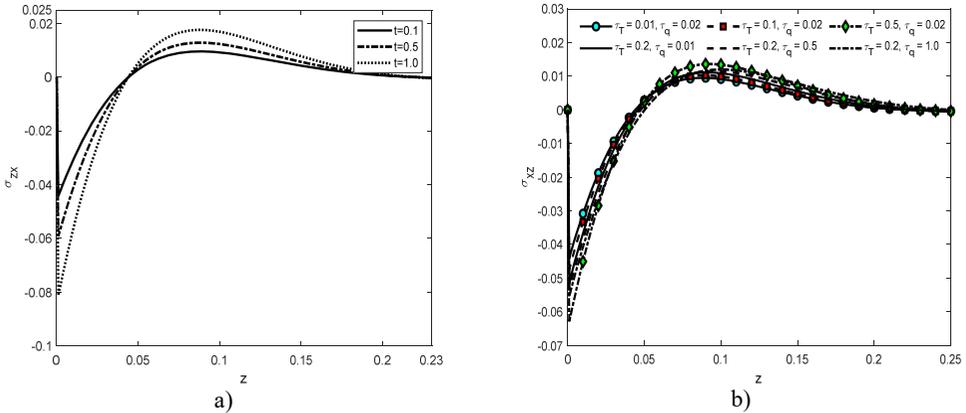
Fig. 5. Micro-temperature 2nd component against different values of time

Propagation of shear stress along the material is presented in the Fig. 7. Just like all other field variables the tangential component of stress has the same response against time parameter of laser pulse. Influences of both the phase-lags  $\tau_T$  and  $\tau_q$  are directly proportional to the wave

propagating through the medium. Highest amplitude is obtained for the value  $\tau_T = 0.2$  and  $\tau_q = 1.0$ .



**Fig. 6.** Normal stress  $\sigma_{zz}$  component against depth for different values of  $t$



**Fig. 7.** Tangential stress  $\sigma_{zx}$  component against depth for different values of  $t$

### 3. Conclusions

Following are some main points which could be concluded after considering the solutions of the problem:

1) Harmonic solution used in Eq. (16) to find the solution of field variables gives analysis of surface waves propagating in the medium. All curves obtained are having non-zero values only in a bounded domain along depth of medium i.e., outside this domain the effects of the waves vanish or converge to zero.

2) The curves obtained during the case of non-dimensional temperature distribution function starts from same initial value depending on selection of  $\theta_0$  in boundary condition. Similarly curves for non-dimensional normal component of stress, and non-dimensional tangential stress starts from zero. These are fully agreement with the physical interpretation of boundary conditions.

3) Time parameter is having decreasing effect on the factor responsible for damping of wave.

4) The phase-lags  $\tau_T$  and  $\tau_q$  are increasing the amplitude of each wave propagating through the medium and having decreasing effect on the damping factor.

5) Curves representing the amplitude of non-dimensional field variables are directly proportional to time parameter. Indicating that greater the value of time parameter, higher the amplitude of wave propagating through the medium. Signifying the fact that laser pulse is having increasing effect on plane wave generated in homogeneous thermoelastic medium in context of

dual-phase-lag heat conduction model as in representation of [25, 26].

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