

Applying deep learning and wavelet transform for predicting the vibration behavior in variable thickness skew composite plates with intermediate elastic support

Wael A. Altabey

International Institute for Urban Systems Engineering (IIUSE), Southeast University, Nanjing, 210096, Jiangsu, China

Department of Mechanical Engineering, Faculty of Engineering, Alexandria University, Alexandria, 21544, Egypt

E-mail: wael.atabey@gmail.com

Received 18 May 2020; received in revised form 20 December 2020; accepted 30 December 2020
DOI <https://doi.org/10.21595/jve.2020.21480>



Copyright © 2021 Wael A. Altabey. This is an open access article distributed under the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited.

Abstract. In this paper, the vibration behavior features are extracted from the combination between Wavelet Transform (WT), and Finite Strip Transition Matrix (FSTM) of skew composite plates (SCPs), with variable thickness, and intermediate elastic support. Although, the results of this technique and based on the previous work done by the authors, that show the method can reflect the vibration behavior of the composite plates. Due to the method's difficulty in terms of, a lot of calculations with a large number of iterations these results may not be good choices for quick and accurate vibration behavior extracting. Thus, the new deep neural network (NN) is designed to learn and test these results carrying out by extracting vibration behavior features that reflect the important and essential information about the mode shapes in SCP. The results give high indications about the proposed technique of deep learning is a promising method, particularly when the type structures are complicated and the ambient environment is variable.

Keywords: free vibration, deep learning, wavelet transform (WT), variable thickness plates, skew composite plates (SCPs), BFRP.

Nomenclature

SCP/SCPs	Skew composite plate/plates
IES	Intermediate elastic support
SP/SPs	skew plate/plates
WT/WTs	Wavelet transform/transforms
FSTM	Finite strip transition matrix
BCs	boundary conditions
CWT	Continuous wavelet transform
MSE	Mean square error
a, b	Length and width of the plate
$h(y)$	Plate thickness as a function of y
h_o, h_b	Plate thickness at $y = 0$ and $y = b$, respectively
h_{ok}	Distance from the middle-plane of the plate according to h_o to the bottom of the h_{oth} layer
m_o	$= \rho h_o$, mass density per unit area of the plate
p	Dynamic load function
$w_o(x, y, z)$	deflection at any point (x, y)
D_{ij}	Plate flexural rigidity
\overline{Q}_{ij}^k	Plane stress transformed reduced stiffness coefficients of the lamina
E	Young's modulus
E_{11}	Longitudinal Young's moduli parallel to the fiber orientation

E_{22}	Transverse Young's moduli perpendicular to the fiber orientation
G_{12}, G_{21}	Plane shear modulus of elasticity
Q	Number of terms used in series solution
N	Number of strips
$W(x, y, z)$	Time-dependent deflection at any point (x, y)
M_n	The normal bending moment at the boundary
X_m	Classical beam functions in the x -direction
Y_n	A series solution in the y -direction
K_T	Elastic restraint coefficient
T	Translational stiffness per unit length
$W(\xi, \eta, t)$	Shape function
$Y_i(\eta)$	Unknown function to be determined
$X_i(\xi)$	Chosen a priori, the basic function in ξ -direction
ν_{12}, ν_{21}	Poisson's ratio
ρ	Density per unit area of the plate
ω	Natural frequency (rad/sec)
ξ, η	= u/a and v/b , respectively, non-Dimensional variables
ϕ	Skew angle
β	= a/b , plate aspect ratio
Δ	= $(h_b - h_o)/h_o, (h_o)$, plate tapered ratio
Ω	$\left(\frac{m_o h(\eta) \omega^2 a^4}{h_o D_{22}}\right)^{1/2}$, non-dimensional frequency parameter (NDFP)
$(\Omega)_{NN}$	Predicted non-dimensional frequency parameter (PNDFP)
n	Number of deep NN data
$\partial w_o / \partial n$	The slope at the boundary
ρ	Material density

1. Introduction

The importance of to use of composite materials in many fields of technology, such as aerospace industries, marine engineering, and civil engineering is due to special features, e.g. high strength/weight ratio and corrosion resistance property, particularly under the effects of the harsh environment. Although the structures are made of these types of materials have some drawback are subject to matrix cracks, fiber breakage, and delamination. These invisible faults can lead to catastrophic structural failures [1-4].

Other major modes of failure of fiber-reinforced polymer (FRP) have a temperature, bending, tensile, stress, impact failure, and failure of the installation, etc. These types of failures are complicated and are not easy to assets, mostly when subjected to associate effects of multiple factors [5-7].

The user of an active system of structural health monitoring (SHM) to observe the safety and potential damage detection in composite plates are essential and most seriously. The function of SHM is consists of three main sub-functions, including system identification, features extraction for algorithms for detection and prediction, and reliability and risk evaluation [8-19].

The vibration behavior of composite structures is the traditional method for the intelligent detecting the defects in the composite. The mode shapes of the structure are one of the essential tools in Structural health monitoring (SHM) in the last decades, where, extracted the vibration response of composite structure for each damage type and position and analysis based on the variance in vibration parameters. In recent years, different techniques to extract the natural frequencies of composite plates have become a field of great interest in the scientific society [20-34].

To find the mode shapes for different boundary conditions with IES, numerical methods or

experimental methods must be used. Some researchers have been interested in the vibration of multi-span plates using different approaches. In previous works, Altabeay [35, 36] used the FSTM as one of the common use of semi-analytical approaches to extract vibration response of basalt FRP laminated variable thickness rectangular plates with IES, and he tried to improve the results accuracy and by the way, decrease the calculations efforts due to a large number of iterations by combined his method with artificial neural networks (ANNs) and response surface (RS) methods.

In the present research, the new deep NN is designed to predict the vibration behavior of SCPs with variable thickness and IES with a different elastic restraint coefficient (K_T) and four cases of boundary conditions (BCs) of plate edges, namely SSSS, CCCC, SSFF, and CCFF. The plate is a rectangular SCP with variable thickness function $h(y)$, the locations of the IES is at mid-line of the presented plate, and the plate was manufactured from basalt fiber reinforced polymer (BFRP) by using five symmetrically layers with the stacking angle $[45^\circ/-45^\circ/45^\circ/-45^\circ/45^\circ]$ as shown in Fig. 1. First, review the illustrated results of the utilized method by the combination of these WT and FSTM methods (WT-FSTM) to convergence the studies by checking the agreement with the results available in the literature. Second, the trained deep NN is used to predict the outcome of the extracted vibration behavior of SCPs from WT-FSTM at certain values of elastic restraint coefficients (K_T) for IES, and then it is subsequently used to predict the vibration behavior for different levels of elastic restraint coefficients (K_T) for IES. The results are predicted from the deep NN model are in very good agreement with the WT-FSTM results. Hence, the results give high indications about the proposed technique of deep learning is a promising method.

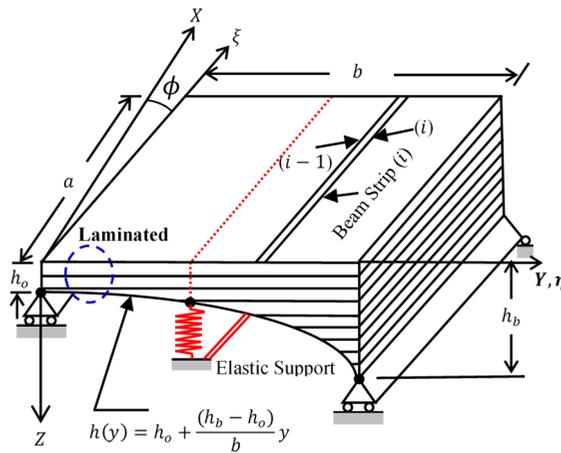


Fig. 1. The geometry of rectangular SCP with variable thickness and IES

2. Model overview

The composite plate material has corresponding elastic and shear modulus values are shown in Table 1.

Table 1. Model property

E_{11} (GPa)	E_{22} (GPa)	ν_{12}	ν_{21}	G_{12} (GPa)	G_{21} (GPa)	rho kg/m ³
96.74	22.55	0.3	0.6	10.64	8.73	2700

The normalized partial differential equation of vibration behavior for the plates system illustrated in Fig.1 under the assumption of the classical deformation theory in terms of the plate deflection $w_o(x, y, t)$ using the non-Dimensional variables ξ and η related to the skew coordinate system (u, v, ϕ) defined by $u = x \sec(\phi)$, $v = y - x \tan(\phi)$, and $\xi = \frac{u}{a}$, $\eta = \frac{v}{b}$, and after some derivation, the governing equation can be written as follows:

$$\begin{aligned}
 & \psi_1 h^3(\eta) \frac{1}{a^4} W_{\xi\xi\xi\xi} - 4\beta(\sin\phi)\psi_3 h^3(\eta) W_{\xi\xi\xi\eta} + \nu\beta^2\psi_2(\cos^2\phi) \frac{\partial^2 h^3(\eta)}{\partial\eta^2} W_{\xi\xi} \\
 & + 2\beta^2\psi_2(\cos^2\phi) \frac{\partial h^3(\eta)}{\partial\eta} W_{\xi\xi\eta} + 2\beta^2\psi_2 h^3(\eta)(3\sin^2\phi + \cos^2\phi) W_{\xi\xi\eta\eta} \\
 & + 2\beta^4(\cos^2\phi) \frac{\partial h^3(\eta)}{\partial\eta} W_{\eta\eta\eta} - 2\beta^3\psi_4\nu(\sin\phi\cos^2\phi) \frac{\partial^2 h^3(\eta)}{\partial\eta^2} W_{\xi\eta} \\
 & - 4\beta^3\psi_4(\sin\phi)h^3(\eta) W_{\xi\eta\eta\eta} + \beta^4(\nu\tan^2\phi + 1)\cos^4\phi \frac{\partial^2 h^3(\eta)}{\partial\eta^2} W_{\eta\eta} \\
 & + \beta^4 h^3(\eta) W_{\eta\eta\eta\eta} - 4\beta^3\psi_4(\sin\phi\cos^2\phi) \frac{\partial h^3(\eta)}{\partial\eta} W_{\xi\eta\eta} = -\Omega^2 h(\eta) h_o^2(\cos^4\phi) W_{tt},
 \end{aligned} \tag{1}$$

where $\psi_1 = \frac{D_{11}}{D_{22}}$, $\psi_2 = \frac{(D_{12}+2D_{66})}{D_{22}}$, $\psi_3 = \frac{D_{16}}{D_{22}}$, $\psi_4 = \frac{D_{26}}{D_{22}}$.

Since the treatment of IES conditions are the main objective of this paper we presented it in more detail. The line of the IES $y = b/2$, the displacement must vanish and the normal moment must be continuous, i.e.

$$K_T w_o = -2\psi_3 \frac{\partial^3 w_o}{\partial x^3} - \frac{\partial^3 w_o}{\partial y^3} - \psi_5 \frac{\partial^2 w_o}{\partial x^2 \partial y} - 4\psi_4 \frac{\partial^3 w_o}{\partial x \partial y^2}, \tag{2}$$

$$\left. \frac{\partial w_o}{\partial y} \right|_{\eta=1^-/2} = \left. \frac{\partial w_o}{\partial y} \right|_{\eta=1^+/2}, \tag{3}$$

where: $\psi_1 = \frac{D_{11}}{D_{22}}$, $\psi_2 = \frac{(D_{12}+2D_{66})}{D_{22}}$, $\psi_3 = \frac{D_{16}}{D_{22}}$, $\psi_4 = \frac{D_{26}}{D_{22}}$, $K_T = \frac{T_{b/2} b^3}{D_{22}}$, $\psi_5 = \frac{(D_{12}+4D_{66})}{D_{22}}$.

3. Determination of vibration behavior using WT and FSTM

In This section, the mode shapes of the SCP will be extracted using a new method by combined between the WT and FSTM methods with an adjusting frequency parameter, in order to improve the estimated accuracy of extracting by optimized the WT entropy for adjusting frequency parameter.

3.1. Continuous wavelet transform (CWT)

Continuous wavelet transform (CWT) is a convolution process of the data sequence with a set of continuous scaled and translated versions of the mother wavelet (MW) $\psi(t)$. The translating process is a smoothing effect over the length of the data sequence to localize the wavelet in time domain $x(t)$, whereas the scaling process is compressing or stretching of analyzed wavelet which indicates various resolutions. The stretched wavelet is used to capture the slow changes; while the compressed wavelet is used to capture abrupt changes in the signal. The trade-off of enhancing resolution is between increased computational cost and memory by computing wavelet components and multiplying each component by the correctly dilated and translated wavelet, resulting in the constituent wavelet of the analyzed signal [37-45].

The $\psi(t)$ is stretched or squeezed through varying its dilation parameter s and moved through its translation parameter τ (i.e. along the localized time index τ):

$$\psi_{s,\tau}(t) = \frac{1}{\sqrt{s}} \psi\left(\frac{t-\tau}{s}\right), \quad \tau \in R, \quad S > 0. \tag{4}$$

Let $x(t)$ be the system shape function response of FSTM, where t denotes time. CWT of a function $x(t) \in L^2(R)$, where $L^2(R)$ is the set of square-integrable functions is denoted as $W_{s,\tau}$

and defined as:

$$W_{s,\tau} = \langle x(t), \psi_{s,\tau}(t) \rangle = \frac{1}{\sqrt{s}} \int_{-\infty}^{-\infty} x(t) \cdot \psi^* \left(\frac{t-\tau}{s} \right) dt, \tag{5}$$

where the wavelet scale s and the period τ are used to adjust the frequency and time location. $W_{s,\tau}$ shows how closely $\psi_{s,\tau}(t)$ correlated with $x(t)$. By inverse CWT, the signal $x(t)$ can be regenerated as:

$$x(t) = \frac{1}{C_\psi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} W_{s,\tau} \psi_{s,\tau} \frac{dsd\tau}{S^2}. \tag{6}$$

For a plate striped in the ξ -direction by divided into N discrete longitudinal strips spanning between supports as shown in Fig. 1, the free-response equation for one striped beam system may be assumed in the form:

$$x(t) = X_i(\xi)Y_i(\eta)e^{j\omega\tau}. \tag{7}$$

The WT of Eq. (7) is:

$$|W_{s_0,\tau}| = \frac{\sqrt{S_0}}{2} X_i(\xi)Y_i(\eta) \cdot \psi^*(S_0\omega)e^{j\omega\tau}. \tag{8}$$

The logarithm of Eq. (8) gives:

$$\ln|W_{s_0,\tau}| = j\omega\tau + \ln \left(\frac{\sqrt{S_0}}{2} X_i(\xi)Y_i(\eta) |\psi^*(S_0\omega)| \right). \tag{9}$$

By using the straight line of the slope of the logarithm of WT modulus, we can be obtained the natural frequency of the system and it is given by:

$$Arg(W_{s_0,\tau}) = \omega\tau \Rightarrow \frac{d}{d\tau} Arg(W_{s_0,\tau}) = \omega. \tag{10}$$

The plot of $\frac{d}{d\tau} Arg(W_{s_0,\tau})$ is constant in the time domain and is equal to the natural frequency ω . The non-dimensional frequency parameter (NDFP) (Ω) are addressed in the form:

$$\Omega = \left(\frac{m_o h(\eta) \omega^2 a^4}{h_o D_{22}} \right)^{1/2}. \tag{11}$$

4. Deep neural networks (NNs)

Recently, deep learning, which is a network with multiple hidden layers of neurons, has also been applied in solving and identifying the ordinary and partial differential equations [46, 47].

Deep neural networks (NNs) are one of the artificial intelligence (AI) algorithms used for solving advanced non-linear problems [48]. The networks are consist of computational nodes that connected together to create one individual network, each node is processing a calculation on input and sends the result to output connections, and maybe a node output is an input to one other node or more.

In this section, we use the outcome of the results in Section 3 of vibration behavior of SCP extracted by WT-FSTM at certain values of elastic restraint coefficients (K_r) to obtain the training

data and to predict the vibration behavior for different levels of elastic restraint coefficients (K_T) not included in the results.

The proposed deep NN architecture connection is presented in Fig. 2. The steps of the NDFP (Ω) prediction can be described through the following steps in Table 2.

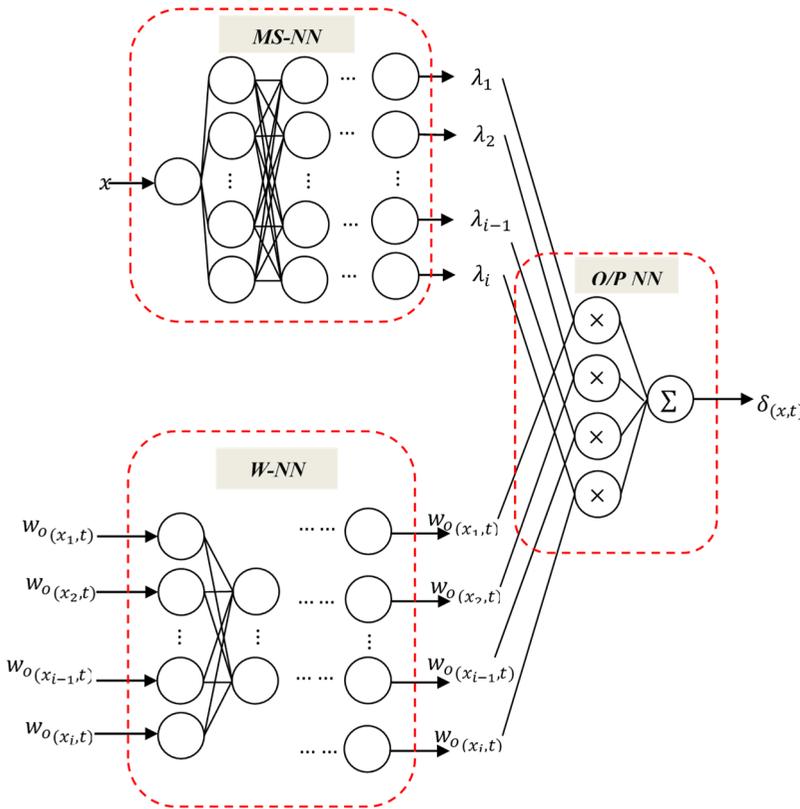


Fig. 2. The architecture of the proposed deep NN for the NDFP (Ω) prediction

Table 2. The steps of deep NN training to predict NDFP (Ω)

NN steps	Step remark
Data collecting	Extract the training data from the WT-FSTM of the SCP at certain values of elastic restraint coefficients (K_T)
Training model	Divide the extracting data into three groups of data, the first one will be used for training in MS-NN for mode shapes λ_i prediction of SCP, and the second group of a dataset will be used for training in W-NN for predicting deflection $w_o(x, t)$, this network without hidden layers
Testing model	The last part of the data will use to test the trained model in the training model. If the model is well-trained, the predicted results by the W-NN and MS-NN will be convergence to the real value. The training performance of suggested Deep NN is presented in Fig. 3
Prediction response	The response MS-NN will be used to predict the λ_i under random deflection $w_o(x, t)$. W-NN will be used to predict the $w_o(x, t)$ at any location coordinate x along with the SCP including the IES location presented in Section 2

It is important for the NN designer to check his proposed deep NN performance is suitable or not from the formula of mean square error (MSE):

$$MSE = \sum \frac{((\Omega)_{NN} - \Omega)^2}{n} \tag{12}$$

Therefore, only one global minimum for performance index based on the features of the input vectors, but the minimum local minimum of a function at finite input values, and it cannot be omitted when attaching deep NN. Therefore, we can judge on accuracy a local minimum, if it has a low closer range to global minimum and low MSE. Anyway, the designer must be selected as a suitable method to solve this problem in order to descent the local minimum with momentum. Momentum allows a network to respond not only to the local gradient but also to recent trends in the error surface. Without momentum, a network may get stuck in a shallow local minimum. Fig. 3 shows the performance curves of training with three groups for learning data.

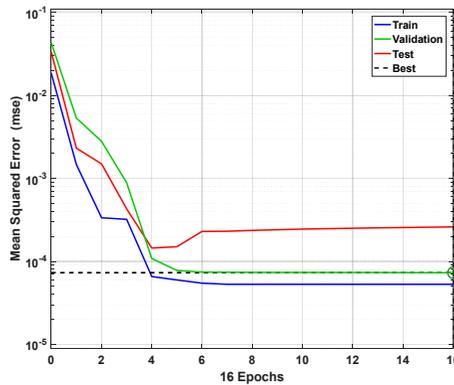


Fig. 3. Training performance of proposed NN

5. Results and discussion

In this section, after reviewing the results available in the literature, the approach of WT-FSTM are used to extract the vibration behavior of SCP with variable thickness are presented in Section 2 at certain values of elastic restraint coefficients (K_T) for IES, on the other hand, to provide the active training data to proposed deep NN, in order to extract the influence of the IES on the natural frequencies with different elastic restraint coefficients (K_T) of such plates.

5.1. Convergence study and accuracy

The importance for review of presented work results with the results available in the literature in order to validate the accuracy and reliability of the proposed technique. In this subsection, the WT-FSTM technique has been applied on a CCCC variable thickness SP with $\beta = 0.5$, $\Delta = (0, 0.2, 0.4, 0.5)$ and $\phi = (30^\circ, 45^\circ, 60^\circ)$, and then the convergence between the results in Fig. 4 with the results from FSTM [35] will be done.

As shown in the Fig. 4, after convergence, we can see clearly generally, that the results of the presented method WT-FSTM in excellent agreement with the other accurate methods in references [23-26, 35]. On the other hand, we can see the effects of plate Skew angles (ϕ), tapered ratio (Δ) and aspect ratio (β) on the NDFP (Ω) it has been increased with increasing of the ϕ , β , and Ω , in all methods WT-FSTM and the methods in the literature.

5.2. Proposed method (WT-FSTM) results

In the present study, the numerical computations using the WT-FSTM approach is applied to extract vibration behavior. Due to the method difficulty in terms of, a lot of calculations with a large number of iterations these results may not be good choices for quickly and accurate vibration

behavior extracting, the new deep NN is designed to learn and test these results carrying out by extracting vibration behavior features that reflect the important and essential information about the mode shapes in SCP. The proposed method target achieved using only two different K_T in computations of the NDFP (Ω), the first one is located at $K_T = 50$ the second is $K_T = 750$, respectively. The first six frequencies are presented in Table 3, the NDFP (Ω) has been computed with different values of skew angle (ϕ) at aspect ratio ($\beta = 0.5$), and tapered ratio ($\Delta = 0.5$) to study the behavior of natural frequencies under a different skew angle for different four BCs namely SSSS, CCCC, SSFF, and CCFF.

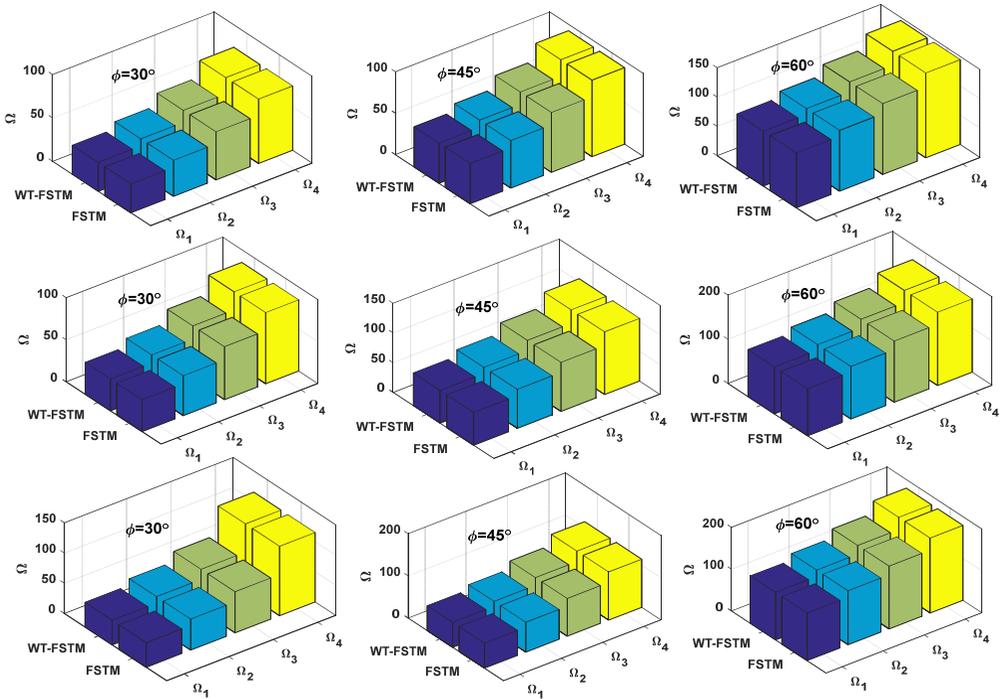
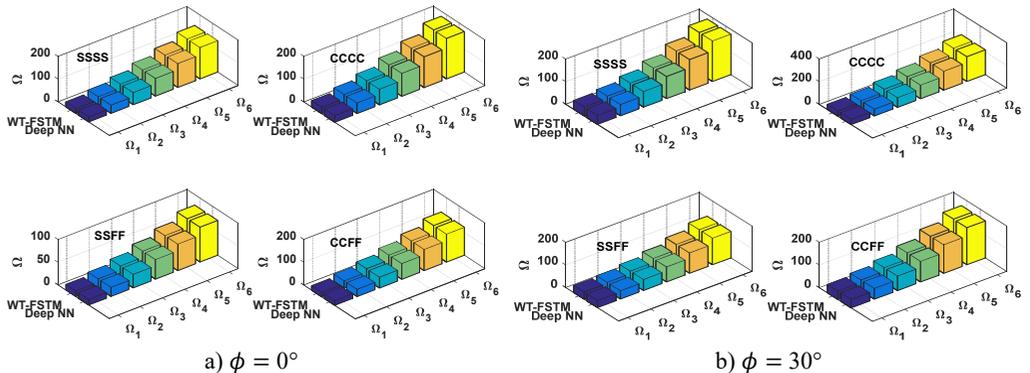


Fig. 4. Comparison of the first four natural frequencies of CCCC skew plates $\beta = 0.5$

Figs. (5-6) represent the comparison between the WT-FSTM data and the deep NN predicted data NDFP (Ω) for $K_T = 50$ and $K_T = 750$ respectively of four different BCs are SSSS, CCCC, SSFF, and CCFF. The results of the proposed deep NN show much satisfactory prediction quality for this case study.



a) $\phi = 0^\circ$

b) $\phi = 30^\circ$

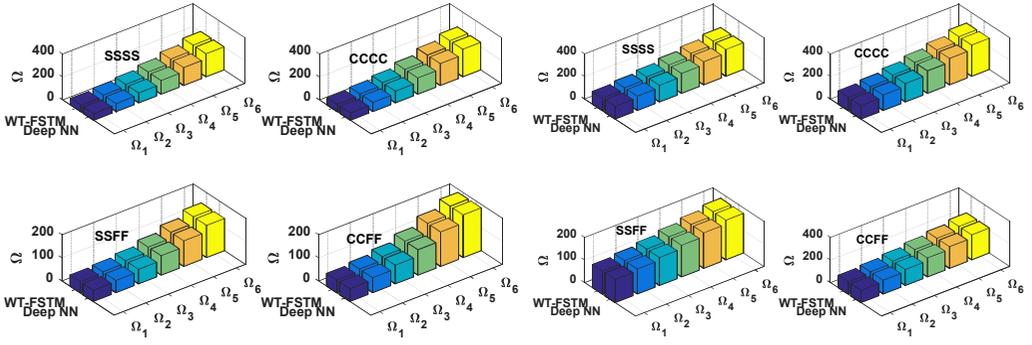


Fig. 5. Comparison between the WT-FSTM data and deep NN predicted data for $K_T = 50$

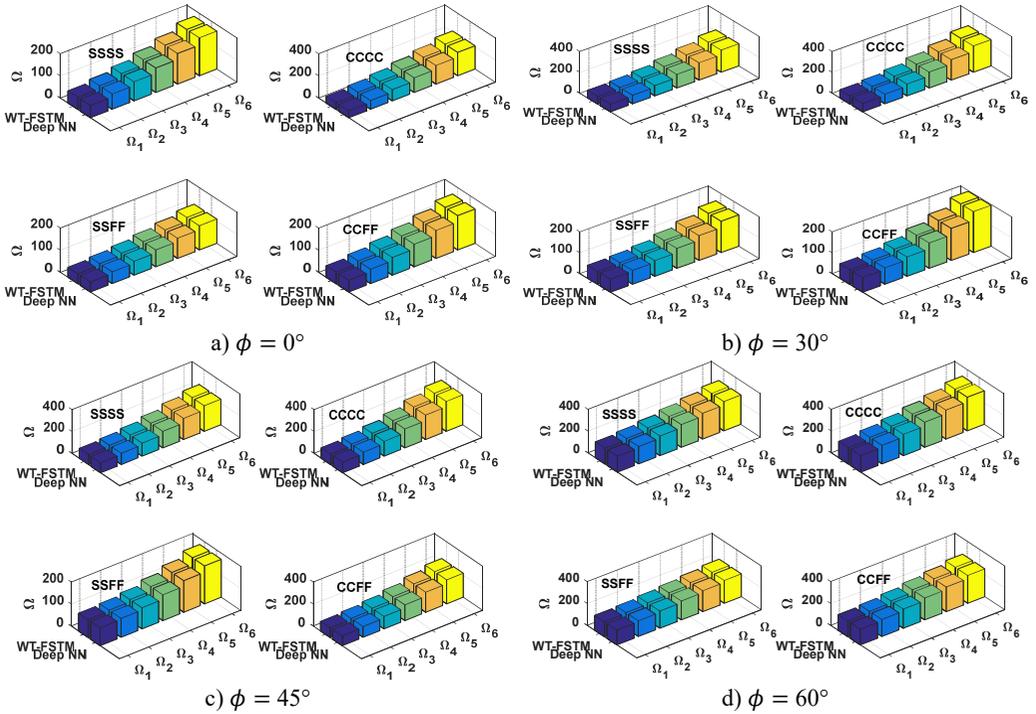


Fig. 6. Comparison between the WT-FSTM data and deep NN predicted data for $K_T = 750$

Table 3. The first six frequencies of SCP, $\beta = 0.5, \Delta = 0.5$

BCs	ϕ	K_T	Ω_1	Ω_2	Ω_3	Ω_4	Ω_5	Ω_6
SSSS	0°	50	22.157	36.232	53.594	78.249	105.594	138.710
		750	55.078	69.159	86.525	111.179	138.523	171.633
	30°	50	39.507	49.713	69.226	98.139	135.487	179.658
		750	72.428	82.640	99.1570	131.069	166.416	212.581
	45°	50	57.936	69.256	87.408	119.321	156.736	201.733
		750	90.857	102.183	120.339	152.251	194.665	234.656
60°	50	112.564	127.407	148.221	177.583	204.928	238.044	
	750	145.485	160.334	181.152	210.513	237.857	270.967	
CCCC	0°	50	28.446	46.511	68.806	100.457	135.565	178.079
		750	61.361	79.435	101.737	133.372	168.490	211.102
	30°	50	45.796	59.992	85.438	120.347	166.458	219.027
		750	78.711	92.916	114.369	153.262	196.383	252.050

	45°	50	64.225	79.535	102.620	141.529	191.707	241.102
		750	97.140	112.459	135.551	174.444	224.632	274.125
	60°	50	118.853	137.686	163.433	199.791	234.899	277.413
		750	151.768	170.610	196.364	232.706	267.824	310.436
SSFF	0°	50	12.286	20.083	29.716	43.375	58.538	76.887
		750	45.206	53.013	62.639	76.305	91.465	109.813
	30°	50	31.636	36.564	48.348	66.265	90.431	117.835
		750	62.556	66.494	75.271	96.195	119.358	150.761
	45°	50	48.065	53.107	63.530	84.447	110.680	139.910
		750	80.985	86.037	96.453	117.377	143.607	172.836
	60°	50	102.693	111.258	124.343	140.709	157.872	176.221
		750	135.613	144.188	157.266	173.639	190.799	209.147
CCFF	0°	50	19.603	32.054	47.423	69.228	93.425	122.724
		750	52.529	64.981	80.346	102.154	126.355	155.641
	30°	50	36.953	47.535	64.055	91.118	126.318	163.672
		750	69.879	78.462	92.978	122.044	154.248	196.589
	45°	50	55.382	65.078	81.237	110.300	149.567	185.747
		750	88.308	98.005	114.160	143.226	182.497	218.664
	60°	50	110.010	123.229	142.050	168.562	192.759	222.058
		750	142.936	156.156	174.973	201.488	225.689	254.975

5.3. Deep NN performance

The performances of suggested deep NN are presented in Table 4 and Fig. 3, the MSE and accuracy of predicted data are calculated from Eq. 12 for NDFP (Ω). From Table 4 and Fig. 3 the value of MSE and accuracy of training data are 7.2 E-5 and 99.7 % respectively and validating data are 6.2 E-5 and 99.8 % respectively. From NN performance shows in Table 4 and Fig. 3, the proposed deep NN gave a good prediction for vibration behavior data in the presented SCP.

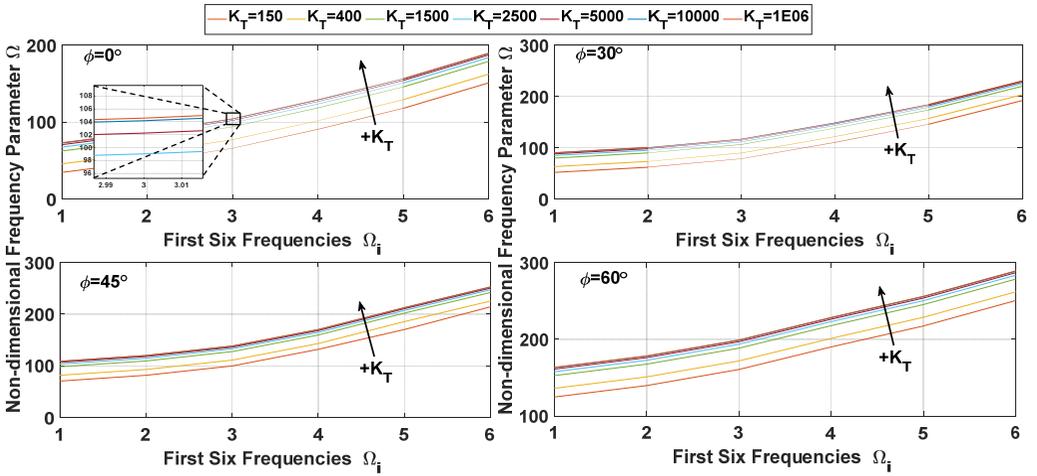
Table 4. Mean square error (MSE) and accuracy values

Data	MSE	Accuracy
Training	7.2 E-5	99.7 %
Validating	6.2 E-5	99.8 %

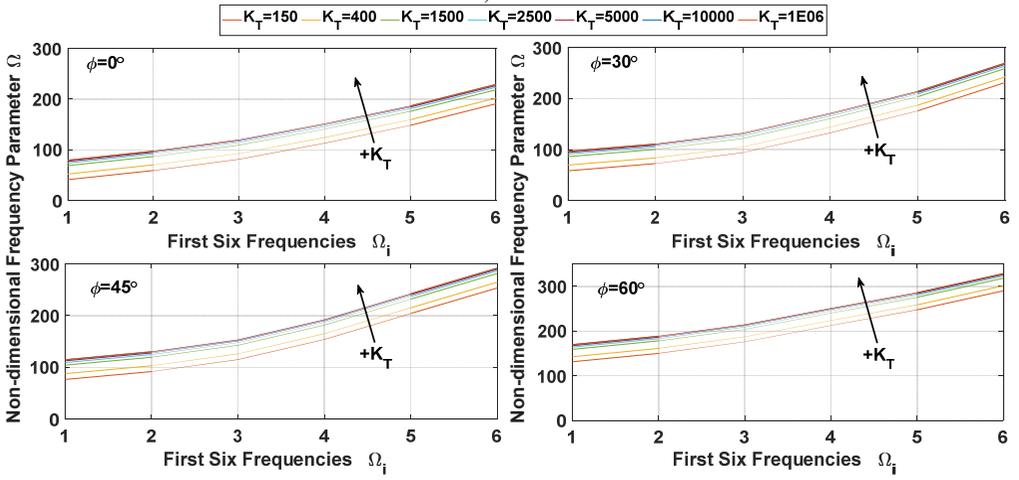
5.4. Deep NN predicting results

In this subsection, the main target of design the deep NN of predicting the vibration behavior data of SCP under different elastic restraint coefficients (K_T) is achieved, chosen 7 different K_T for different four BCs (SSSS, CCCC, SSFF, and CCFF). The deep NN predicted results of the first six frequencies of SCP with $\beta = 0.5$ and $\Delta = 0.5$ are shows in Fig. 7.

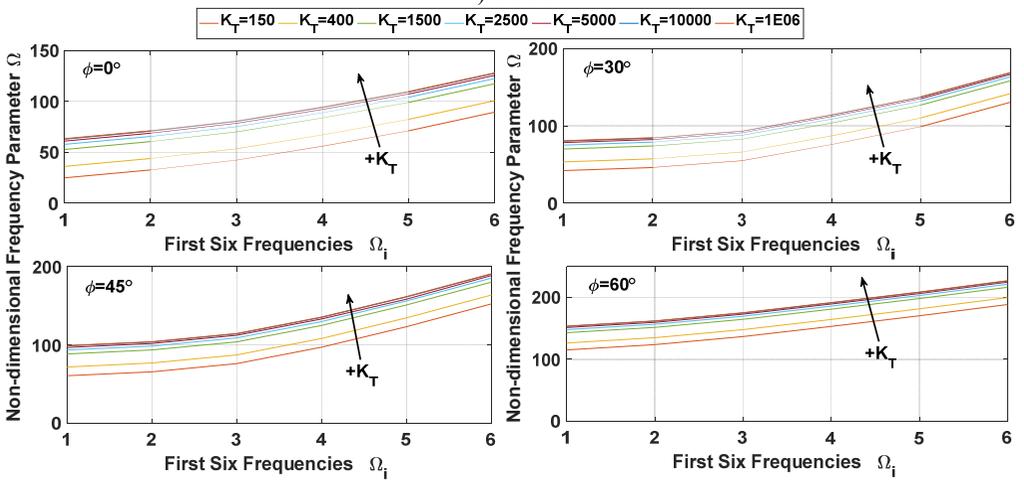
Moreover, the influence of the IES on the vibration behavior of the SCPs with variable thickness is shown in Fig. 7. As shown in the Fig. 7 for all values of skew angle (ϕ) and all types of BCs, the first six frequencies are increasing with increasing of the value of elastic restraint coefficient (K_T). whereas the frequencies rapidly increase with for small values of elastic restraint coefficient (K_T), and the influence of IES becomes negligible at high values. On the other hand for all values of skew angle (ϕ), the first six frequencies for fully clamped (CCCC) plate are the highest frequencies, and the semi-simply supported (SSFF) plate is the lowest one, while, the other two boundaries (SSSS and CCFF) were rested between them. also, we can see the effects of plate skew angles (ϕ) on the NDFP (Ω) it has been increased with increasing of the. skew angles.



a) SSSS



b) CCCC



c) SSFF

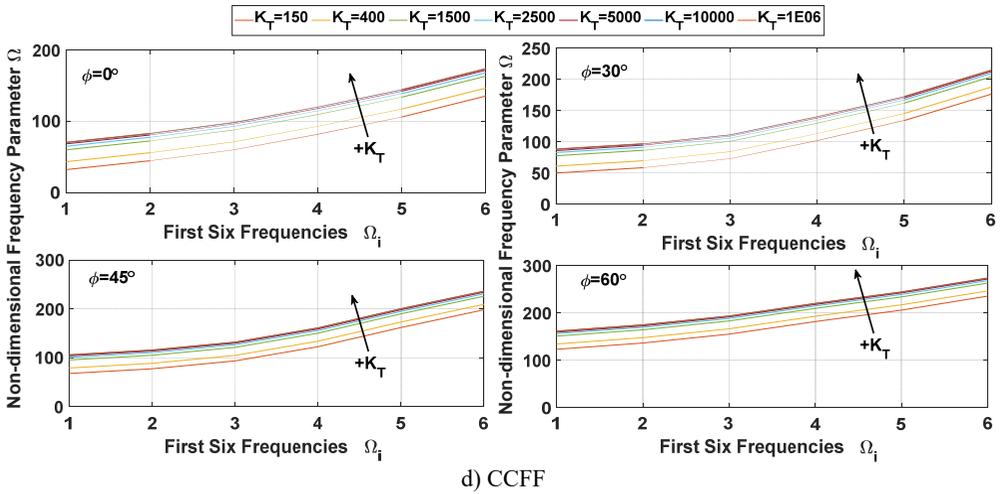


Fig. 7. The deep NN predicted results of NDFP (Ω)

6. Conclusions

By a combination of the WT and FSTM method (WT-FSTM) was used to extract the vibration behavior of SCP with variable thickness, and IES, the plate is made from BFRP laminated. First, To investigate from accuracy and reliability of the proposed technique, the convergence between the proposed study results with the results available in the literature has been checked, thus validating the accuracy and reliability of the proposed technique. Then, due to the proposed method's difficulty in terms of, a lot of calculations with a large number of iterations, these results may not be good choices for quick and accurate vibration behavior extracting. Thus, the new deep neural network (NN) is designed to learn and test these results carrying out by extracting vibration behavior features that reflect the important and essential information about the mode shapes in SCP. The influence of β , Δ , ϕ , and K_T on the predicted NDFP (Ω) of the plate, has been studied, with four different support conditions (SSSS, CCCC, SSFF, and CCFE).

Based on the WT-FSTM and the deep NN predicted results, we conclude that the deep NN predicted results of NDFP (Ω) are in very good agreement with the proposed method results WT-FSTM with an accuracy of training and validating data are 99.7 % and 99.8 % respectively.

References

- [1] Zhao Y., Noori M., Altabey W. A., Ghiasi R., Wu Z. A fatigue damage model for FRP composite laminate systems based on stiffness reduction. *Structural Durability and Health Monitoring*, Vol. 13, Issue 1, 2019, p. 85-103.
- [2] Zhao Y., Noori M., Altabey W. A., Naiwei L. Reliability evaluation of a laminate composite plate under distributed pressure using a hybrid response surface method. *International Journal of Reliability, Quality and Safety Engineering*, Vol. 24, Issue 3, 2017, p. 1750013.
- [3] Altabey W. A., Noori M. Fatigue life prediction for carbon fibre/epoxy laminate composites under spectrum loading using two different neural network architectures. *International Journal of Sustainable Materials and Structural Systems (IJSMS)*, Vol. 3, Issue 1, 2017, p. 53-78.
- [4] Wang T., Noori M., Altabey W. A. Identification of cracks in an Euler-Bernoulli beam using bayesian inference and closed-form solution of vibration modes. *Proceedings of the Institution of Mechanical Engineers, Part L: Journal of Materials: Design and Applications*, 2020, <https://doi.org/10.1177/1464420720969719>.
- [5] Altabey W. A. An exact solution for mechanical behavior of BFRP Nano-thin films embedded in NEMS. *Advances in Nano Research*, Vol. 5, Issue 4, 2017, p. 337-357.
- [6] Altabey W. A. A study on thermo-mechanical behavior of MCD through bulge test analysis. *Advances in Computational Design*, Vol. 2, Issue 2, 2017, p. 107-119.

- [7] **Ghannadi P., Kourehli S. S., Noori M., Altabey W. A.** Efficiency of grey wolf optimization algorithm for damage detection of skeletal structures via expanded mode shapes. *Advances in Structural Engineering*, Vol. 23, Issue 13, 2020, p. 2850-2865.
- [8] **Ghiasi R., Ghasemi M. R., Noori M., Altabey W. A.** A non-parametric approach toward structural health monitoring for processing big data collected from the sensor network. *Structural Health Monitoring*, 2019.
- [9] **Altabey W. A.** Detecting and predicting the crude oil type inside composite pipes using ECS and ANN. *Structural Monitoring and Maintenance*, Vol. 3, Issue 4, 2016, p. 377-393.
- [10] **Altabey W. A.** FE and ANN model of ECS to simulate the pipelines suffer from internal corrosion. *Structural Monitoring and Maintenance*, Vol. 3, Issue 3, 2016, p. 297-314.
- [11] **Altabey W. A., Noori M.** Detection of fatigue crack in basalt FRP laminate composite pipe using electrical potential change method. *Journal of Physics: Conference Series*, Vol. 842, 2017, p. 012079.
- [12] **Zhao Y., Noori M., Altabey W. A., Zhishen W.** Fatigue damage identification for composite pipeline systems using electrical capacitance sensors. *Smart Materials and Structures*, Vol. 27, Issue 8, 2018, p. 085023.
- [13] **Altabey W. A.** Delamination evaluation on basalt FRP composite pipe by electrical potential change. *Advances in Aircraft and Spacecraft Science*, Vol. 4, Issue 5, 2017, p. 515-28.
- [14] **Altabey W. A.** EPC method for delamination assessment of basalt FRP pipe: electrodes number effect. *Structural Monitoring and Maintenance*, Vol. 4, Issue 1, 2017, p. 69-84.
- [15] **Altabey W. A., Noori M., Alarjani A., Zhao Y.** Nano-delamination monitoring of BFRP nano-pipes of electrical potential change with ANNs. *Advances in Nano Research*, Vol. 9, Issue 1, 2020, p. 1-13.
- [16] **Altabey W. A., Noori M., Alarjani A., Zhao Y.** Tensile creep monitoring of basalt fiber-reinforced polymer plates via electrical potential change and artificial neural network. *Scientia Iranica, Transactions on Mechanical Engineering (B)*, Vol. 27, Issue 4, 2020, p. 1995-2008.
- [17] **Altabey W. A.** The thermal effect on electrical capacitance sensor for two-phase flow monitoring. *Structural Monitoring and Maintenance*, Vol. 3, Issue 4, 2016, p. 335-347.
- [18] **Altabey W. A.** An exact solution for acoustic simulation based transmission loss optimization of double-chamber silencer. *Journal of Sound and Vibration (SV)*, Vol. 54, Issue 4, 2020, p. 215-224.
- [19] **Ghiasi R., Noori M., Altabey W. A., Silik A., Wang T., Zhishen W.** Uncertainty handling in structural damage detection via non-probabilistic meta-models and interval mathematics, a data-analytics approach. *Applied Sciences*, Vol. 11, Issue 2, 2021, p. 770, <https://doi.org/10.3390/app11020770>.
- [20] **Laura P. A. A., Grossi R. O., Soni S. R.** Free vibrations of a rectangular plate of variable thickness elastically restrained against rotation along three edges and free on the fourth edge. *Journal of Sound and Vibration*, Vol. 62, 1979, p. 493-503.
- [21] **Mukhopadhyay M.** Free vibration of rectangular plates with edges having different degrees of rotational restraint. *Journal of Sound and Vibration*, Vol. 67, Issue 4, 1979, p. 459-468.
- [22] **Malhotra S. K., Ganesan N., Veluswami M. A.** Vibration of orthotropic square plate having variable thickness (Parabolic Shape). *Journal of Sound and Vibration*, Vol. 119, 1987, p. 184-188.
- [23] **Dokainish M. A., Kumar K.** Vibration of orthotropic parallaogramic plates with variable thickness, *AIAA Journal*, Vol. 11, 1973, p. 1618-1621.
- [24] **Bardell N. S.** The free vibration of skew plates using the hierarchical finite element method. *Journal of Computers and Structures*, Vol. 45, 1992, p. 841-874.
- [25] **Singh B., Saxena V.** Transverse vibration of skew plate with variable thickness. *Journal of Sound and Vibration*, Vol. 206, 1997, p. 1-13.
- [26] **Mizusawa T., Kajita T., Naruoka M.** Vibration of skew plates by using B-Spline functions. *Journal of Sound and Vibration*, Vol. 62, 1979, p. 301-308.
- [27] **Chopra I., Durvasula S.** Natural frequencies and modes of tapered skew plates. *International Journal of Mechanical Sciences*, Vol. 13, 1971, p. 935-944.
- [28] **Liu W. H., Chang I. B.** Vibration of non-uniform skewed cantilever plates by the method of finite element transfer matrix. *Journal of Sound and Vibration*, Vol. 136, 1990, p. 157-163.
- [29] **Garg A. K., Khare R. K., Kant T.** Free vibration of skew fiber reinforced composite and sandwich laminates using a shear deformable finite element model. *Journal of Sandwich Structures and Materials*, Vol. 8, 2006, p. 33-52.
- [30] **Li Z., Noori M., Altabey W. A.** An experimental study on the seismic performance of adobe walls. *Structural Durability and Health Monitoring*, 2020, (in press).
- [31] **Zhao Y., Noori M., Altabey W. A.** Reaching law based sliding mode control for a frame structure under seismic load. *Journal of Earthquake Engineering and Engineering Vibration*, Vol. 20, Issue 1, 2021, p. 25-37, <https://doi.org/10.1007/s11803-021-2003-1>.

- [32] **Narjabadifam P., Hoseinpour R., Noori M., Altabe W.** Practical seismic resilience evaluation and crisis management planning through GIS-based vulnerability assessment of buildings. *Journal of Earthquake Engineering and Engineering Vibration*, Vol. 20, Issue 2, 2021, p. 25-37, <https://doi.org/10.1007/s11803-021-2003-1>.
- [33] **Setoodeh A. R., Karami G. A.** A solution for the vibration and buckling of composite laminates with elastically restrained edges. *Journal of Computers and Structures*, Vol. 60, 2003, p. 245-253.
- [34] **Cheung Y. K., Zhou D.** Vibration analysis of Symmetrically Laminated rectangular plates with intermediate line supports. *Journal of Computer and Structures*, Vol. 79, 2001, p. 33-41.
- [35] **Al-Tabey W. A.** Vibration Analysis of Laminated Composite Variable Thickness Plate Using Finite Strip Transition Matrix Technique and MATLAB Verifications. Chapter 21, InTech, 2014, p. 283-620.
- [36] **Altabe W. A.** Prediction of natural frequency of basalt fiber reinforced polymer (FRP) laminated variable thickness plates with intermediate elastic support using artificial neural networks (ANNs) method. *Journal of Vibroengineering*, Vol. 19, Issue 5, 2017, p. 3668-3678.
- [37] **Noori M., Haifegn W., Altabe W. A., Ahmad I. H. S.** A modified wavelet energy rate based damage identification method for steel bridges. *Scientia Iranica, International Journal of Science and Technology, Transactions on Mechanical Engineering (B)*, Vol. 25, Issue 6, 2018, p. 3210-3230.
- [38] **Zhao Y., Noori M., Altabe W. A., Seyed B. B.** Mode shape based damage identification for a reinforced concrete beam using wavelet coefficient differences and multi-resolution analysis. *Journal of Structural Control and Health Monitoring*, Vol. 25, Issue 3, 2017, p. e2041.
- [39] **Zhao Y., Noori M., Altabe W. A.** Damage detection for a beam under transient excitation via three different algorithms. *Journal of Structural Engineering and Mechanics*, Vol. 63, Issue 6, 2017, p. 803-817.
- [40] **Zhao Y., Noori M., Altabe W. A., Awad T.** A Comparison of three different methods for the identification of hysterically degrading structures using BWBN model. *Journal of Frontiers in Built Environment*, 2019, Vol. 4, p. 80.
- [41] **Silik A., Noori M., Altabe W. A., Ghiasi R.** Comparative analysis of wavelet transform for time-frequency analysis and transient localization in structural health monitoring. *Journal of Structural Durability and Health Monitoring*, 2020, (in press).
- [42] **Silik A., Noori M., Altabe W. A., Ghiasi R.** Choosing optimum levels of wavelet multi-resolution analysis for time-varying signals in structural health monitoring. *Journal of Structural Control and Health Monitoring*, 2020, (in press).
- [43] **Ashory M. R., Khatibi M. M., Jafari M., Malekjafarian A.** Determination of mode shapes using wavelet transform of free vibration data. *Journal of Archive of Applied Mechanics*, Vol. 83, 2013, p. 907-921.
- [44] **Miranda F. J.** Wavelet analysis of lightning return stroke. *Journal of Atmospheric and Solar-Terrestrial Physics*, Vol. 70, Issues 11-12, 2008, p. 1401-1407.
- [45] **Kumar R., Ismail M., Zhao W., Noori M., Yadav A. R., Chen S., Singh V., Altabe W. A., Silik A. I. H., Kumar G., Kumar J., Balodi A.** Damage detection of wind turbine system based on signal processing approach: a critical review. *Journal of Clean Technologies and Environmental Policy*, 2021, <https://doi.org/10.1007/s10098-020-02003-w>.
- [46] **Wang T., Altabe W. A., Noori M., Ghiasi R.** A deep learning based approach for response prediction of beam-like structures. *Structural Durability and Health Monitoring*, Vol. 14, Issue 4, 2020, p. 315-338.
- [47] **Kost A., Altabe W. A., Noori M., Awad T.** Applying neural networks for tire pressure monitoring systems. *Structural Durability and Health Monitoring*, Vol. 13, Issue 3, 2019, p. 247-266.
- [48] **Zhao Y., Noori M., Altabe W. A., Ghiasi R., Wu Z.** Deep learning-based damage, load and support identification for a composite pipeline by extracting modal macro strains from dynamic excitations. *Journal of Applied Sciences*, 2018, Vol. 8, Issue 12, p. 2564.



Wael A. Altabe has been an Associate Professor of mechanical engineering, Faculty of Engineering, Alexandria University, Alexandria, Egypt. He is currently an associate researcher and visiting scholar at Engineering Mechanics, in Southeast University, Nanjing, China. He was awarded a postdoctoral research certificate in 2018, from Southeast University, Nanjing, China, after completing a post-doctoral research fellowship for two years, in SHM and damage detection. Dr. Altabe received his Ph.D. in 2015 in the area of fatigue of composite structures and his M.Sc., 2009, in dynamic systems and his B.Sc., 2004, in Mechanical Engineering, from Mechanical Engineering Department, Faculty of Engineering, Alexandria University.