

Study on compressing principle of the fresh municipal solid waste

Yongneng Lu¹, Erfei Zhao², Zhenping Zhou³, Mingwei Wang⁴

¹State Key Laboratory of Intelligent Manufacturing of Advanced Construction Machinery, Xuzhou Construction Machinery Group, Xuzhou, China

¹Jiangsu Xuzhou Construction Machinery Research Institute, Xuzhou, China

^{2,3,4}School of Mechanical and Aerospace Engineering, Jilin University, Changchun, China

²Corresponding author

E-mail: ¹luyn0217@163.com, ²zhaoerfei@jlu.edu.cn, ³zhouzp@jlu.edu.cn, ⁴271422606@qq.com

Received 31 May 2019; accepted 10 July 2019

DOI <https://doi.org/10.21595/vp.2019.20837>



Copyright © 2019 Yongneng Lu, et al. This is an open access article distributed under the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited.

Abstract. Compression garbage trucks mainly work on fresh municipal solid waste (MSW), while fresh MSW has complex composition, high compressibility, high water content. Less research has been done about fresh MSW. Its uncertain mechanical property limits the simulation of garbage compression process, thereby limits the compressor structure analysis and optimization for compression garbage trucks. In order to obtain the mechanical properties of fresh MSW, a special test device combining the direct shear test with the confined compression test was designed, manufactured and assembled. A total fifteen tests from four batches fresh MSW were conducted with the special test devices. And the Duncan-Chang constitutive model parameters by summarizing and organizing test data. Finally, the confined compression test was simulated with the constitutive model, and the constitutive model parameters was verified. The research provides a basis for the simulation of garbage compression process of the compression garbage truck.

Keywords: compression garbage truck, fresh municipal solid waste (MSW), Duncan-Chang constitutive model, direct shear test, confined compression test.

1. Introduction

China's urban waste production was increasing at an annual rate of 8 % to 10 % in recent years. Finding a proper way to dispose of municipal solid waste has become an urgent problem for urban development [1]. Driven by national policy and rigid demand, total amount of the sanitation market will maintain a rapid growth of more than 20 % in the next five years. And with the improvement of people's awareness of energy conservation and environmental protection, compression garbage trucks with hermetic, self-compression and large loading capacity are more and more accepted by the public, and their occupation rate in garbage trucks will increase gradually.

Fresh MSW consists of many different components, including waste paper, vegetables, peels, wood, grass, leaves, textiles, bones, plastics, rubber, metal, brick, stone, earth, ceramics, glass, and so on. In addition, the water content is also very large. These ingredients are usually porous and unsaturated, which have a significant impact on the engineering properties of domestic waste [2, 3]. Zhang et al. [4] conducted a combined compression and direct shear test on fresh domestic waste, and studied its strength characteristics under different compressive strains systematically. Zhang [5] used the unidirectional compression test and the direct shear test results to propose a simplified calculation method for the Duncan-Chang model parameter of the garbage, and obtained the Duncan-Chang model parameter of the garbage.

The main working object of compression garbage trucks is fresh MSW. Peng Xuan et al. [6] used Zhang's Duncan-Chang model parameters of landfill waste [5] to analyze the structure of garbage compression vehicles. In order to improve the performance and optimize structure of compression garbage trucks, it's indispensable to simulate the compression device [7]. However, it is very difficult to implemented due to the uncertainty of the mechanical properties of the

garbage.

Therefore, it is urgent to carry out experimental research to obtain actual mechanical properties of fresh MSW, and provide a basis for the design technology of compression garbage trucks and other waste processing equipment. Duncan-Chang model was chosen as constitutive model of fresh MSW, and a special test device was designed, manufactured and assembled to conduct tests of fresh MSW. The parameters of Duncan-Chang constitutive model were achieved by data processing. Last, garbage compression process was simulated with the Duncan-Chang constitutive model.

2. Duncan-Chang model and test devices

2.1. Duncan-Chang $E - \mu$ constitutive model

Until now, domestic and international scholars proposed countless soil constitutive models, and the Duncan-Chang model is one of them. In the conventional triaxial test, the axial stress σ_1 is applied when the σ_3 is unchanged. At this time, the stress increment is applied in only one direction, and the stress increments of the other directions are unchanged. The Duncan-Chang model starts from this point [8]. The model is a nonlinear elastic model based on the incremental generalized Hooke's law. It can reflect the nonlinearity of the stress-strain relationship with only 8 parameters, and every parameter has clear physical meaning, so it's easy to grasp. It can be determined by static triaxial test, and is easy to be used in numerical calculation, therefore, it has been used widely [9, 10].

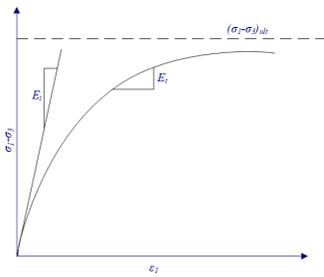


Fig. 1. The relation between $\sigma_1 - \sigma_3$ and ε_1

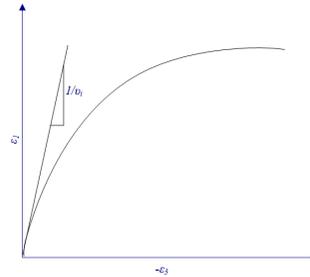


Fig. 2. The relation of ε_1 and ε_3

The relationship between $\sigma_1 - \sigma_3$ and axial strain ε_1 can be represented with a hyperbola, as shown in Fig. 1. The relationship between axial strain ε_1 and the confined strain ε_3 can also be represented with a hyperbola, as shown in Fig. 2.

The tangent elastic modulus E_t at any stress (σ_1, σ_3) is shown in Eq. (1) [8]:

$$E_t = \left[1 - \frac{R_f(\sigma_1 - \sigma_3)(1 - \sin \varphi)}{2c \cos \varphi + 2\sigma_3 \sin \varphi} \right]^2 E_i, \quad (1)$$

where, initial tangent elastic modulus $E_i = K p_a (\sigma_3 / p_a)^n$; K is coefficient of elastic modulus; n is exponent of elastic modulus; p_a is atmospheric pressure; σ_3 is minor principal stress or confining pressure; c is cohesion; φ is internal friction angle; R_f is damage ratio.

The tangent Poisson's ratio μ_t at any stress (σ_1, σ_3) is shown in Eq. (2):

$$\mu_t = \frac{\mu_i}{\left\{ 1 - \frac{D(\sigma_1 - \sigma_3)}{E_i \left[1 - \frac{R_f(\sigma_1 - \sigma_3)(1 - \sin \varphi)}{2c \cos \varphi + 2\sigma_3 \sin \varphi} \right]} \right\}^2}, \quad (2)$$

where, initial Poisson's ratio $\mu_i = G - F \lg(\sigma_3/p_a)$, G , F and D are the undetermined parameters of the initial Poisson's ratio.

To summarize, the eight parameters of Duncan-Chang constitutive model are cohesion c , internal friction angle φ , damage ratio R_f , elastic modulus coefficient K , elastic modulus exponent n , undetermined parameter of the tangent Poisson's ratio G , F and D . The Duncan-Chang constitutive model parameters are generally obtained through triaxial tests. But maintaining confining pressure σ_3 in triaxial test device is very difficult and needs lot of auxiliary devices. Meanwhile, almost all scales of triaxial test devices are small, and they are not suitable to conduct garbage compression test due to uneven composition. It's difficult and costly to develop large scale triaxial test devices. Zhang [5] proposed a simplified calculation method, in which Duncan-Chang model can be put out by the results of direct shearing test and the axial direction compression test.

2.2. Direct shear test

The direct shear test is a common method for determining the shear strength in soil mechanics. The shear stress at the horizontal plane failure can be obtained from horizontal shear force to the samples under different vertical pressures. And cohesion c , internal friction angle φ can be calculated further according to the Coulomb strength theory. According to Zhang's suggestion [5], we used the slow shear test of the direct shear test, and cohesion c , internal friction angle φ were taken as the parameters of the Duncan-Chang model when the shear strain reached 10%. The relation between normal stress σ and shear stress τ_f is shown in Coulomb equation Eq. (3):

$$\tau_f = c + \sigma \cdot \text{tg}\varphi. \quad (3)$$

Taking the shear stress τ_f as ordinate and the normal stress σ as abscissa, the relationship between the shear stress and the normal stress is plotted in Fig. 3. The intercept of the line on the ordinate is cohesion c and the inclination of the line is the internal friction angle φ , as shown in Fig. 3.

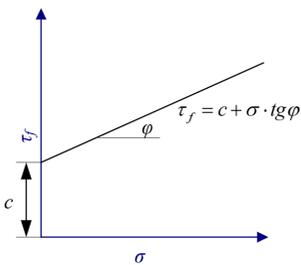


Fig. 3. Principle of direct shear test

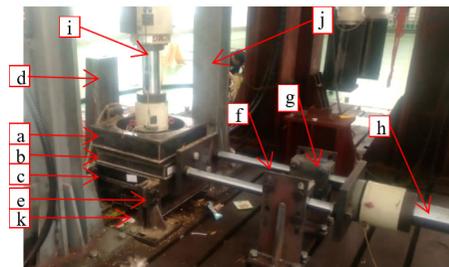


Fig. 4. Direct shear test device: a – upper bucket; b – middle bucket; c – lower bucket; d – upper bucket support; e – lower bucket support; f – horizontal slide; g – horizontal slide support; h – horizontal actuator; i – vertical actuator; j – vertical cylinder fixed frame; k – sewage tank

A large-scale test device was needed, so inner diameter of the test device was set to 500 mm. The container of traditional direct shear device is generally composed of two parts, one shear surface, which needs to overcome the friction of the sample and the weight of the counterweight. In order to improve the accuracy of the shear test, the container we designed was divided into three parts: upper, middle and lower parts. The shear force is applied to the middle part to achieve the shear of the sample. The upper and lower buckets were fixed completely, while the middle bucket was connected to the horizontal hydraulic actuator through the horizontal slides. Vertical pressure was provided by the vertical hydraulic actuator and horizontal shear is provided by the

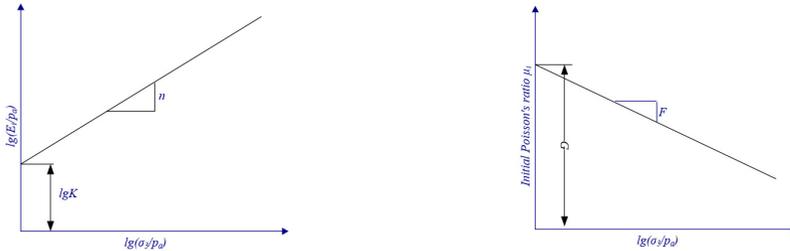
horizontal actuator. The fresh MSW has a large water content, and a large amount of sewage was continuously discharged during the compression process. So some holes with diameter of 5 mm were arranged at the bottom of the lower bucket for the sewage discharge to sewage tank. The special direct shear device is shown in Fig. 4.

2.3. Confined compression test device

Take the logarithm of initial elastic modulus E_i on both sides:

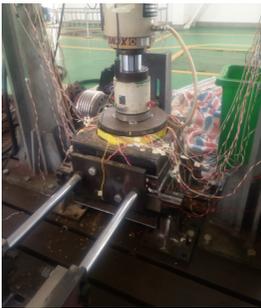
$$\lg\left(\frac{E_i}{p_a}\right) = \lg K + n \lg\left(\frac{\sigma_3}{p_a}\right). \quad (4)$$

Taking $\lg(E_i/p_a)$ as ordinate and $\lg(\sigma_3/p_a)$ as abscissa, the line is plotted as Fig. 5(a). Then the intercept is $\lg K$ and the slope is the elastic modulus exponent n . This is the method to determine Duncan-Chang model parameters K and n with the triaxial test. According to the initial Poisson's ratio μ_i , taking μ_i as ordinate and $\lg(\sigma_3/p_a)$ as abscissa, the line is plotted as shown in Fig. 5(b). Then the intercept is G and the slope is F . This is the method to determine Duncan-Chang model parameters G and F with the triaxial test.



a) The relation between $\lg(E_i/p_a)$ and $\lg(\sigma_3/p_a)$ b) the relation between μ_i and $\lg(\sigma_3/p_a)$

Fig. 5. Principle of confined compression test



a) Overall view of the confined test device b) Strain gauges on outer surface of thin-walled bucket

Fig. 6. Confined compression test device

Confined compression test device was reformed on the basis of the direct shear test device. The upper bucket, middle bucket and lower bucket were kept aligned vertically, and the horizontal actuator was locked. Another thin wall bucket with inner diameter of 476 mm, height of 500 mm and thickness of 2 mm was laid in bucket to conduct the confined compression test, as shown in Fig. 6(a). Seven rows and eight columns of strain gauges were arranged on outer surface of thin wall bucket, and their direction is the circumferential tangential direction, as shown in Fig. 6(b). In the compression process, V402EX wireless dynamic strain test system was used to monitor the microstrain value ε_φ of each strain gauge, so that the circumferential tangential stress σ_φ can be obtained as shown in Eq. (5):

$$\sigma_{\varphi} = E\varepsilon_{\varphi}/10^6, \tag{5}$$

where, E is the elastic modulus of the thin-walled bucket.

Since the wall thickness is much smaller than the radius, the relationship between the circumferential stress σ_{φ} and the internal pressure σ_3 of the thin-walled bucket can be obtained according to the elastic mechanics equation Eq. (6):

$$\sigma_{\varphi} = \sigma_3 R/t, \tag{6}$$

where, R and t are inner diameter and wall thickness of the thin-walled bucket.

Therefore, the confining pressure σ_3 can be derived as Eq. (7):

$$\sigma_3 = \frac{t E \varepsilon_{\varphi}}{R 10^6}. \tag{7}$$

In this way, the confining pressure σ_3 of the garbage can be derived by the microstrain values ε_{φ} of these strain gauges.

3. Test data and final Duncan-Chang constitutive model

3.1. Direct shear test data and confined compression test data

The direct shear test data was processed according to Eq. (3), and the points of normal compression stress σ and shear stress τ_f are plotted shown in Fig. 3. The straight line was fitted to obtain the internal friction angle φ and the cohesion c .

The confined test data were processed according to Eq. 4, and the elastic modulus coefficient K and exponent n were obtained by linear fitting as shown in Fig. 5(a). According to Eq. (4), the data of confined compression test were processed and the coefficient G and F were obtained by linear fitting, as shown in Fig. 5(b).

3.2. The final Duncan-Chang constitutive model parameters

According to Feng’s research [11], the damage ratio R_f of garbage increases with the axial strain. Meanwhile, it is recommended to take $\varepsilon = 10\%$ as damage standard of the garbage, and take the damage ratio $R_f = 0.55$ without triaxial test data. The final Duncan-Chang constitutive model parameters of the fresh MSW were taken the average, as shown in Table 1.

Table 1. The final Duncan-Chang model parameters of the fresh MSW

Constitutive model parameters	Value	Obtaining method
Cohesion c	8 kPa	Direct shear test
Internal friction angle φ	12°	Direct shear test
Damage ratio R_f	0.55	Reference [11]
Modulus of elasticity K	6	Confined compression test
Elastic modulus exponent n	1.15	Confined compression test
G	0.39	Confined compression test
F	0.0166	Confined compression test
D	1	Reference [5]

4. Simulation of garbage compression process

4.1. Model of confined compression test

Based on the Duncan-Chang constitutive model of fresh MSW obtained in the previous article,

simulation of garbage compression test was conducted with ANSYS. But all FEA software lacks Duncan-Chang constitutive model, so further development is achieved with the APDL language on ANSYS platform. The material properties of every element are constantly changing in Duncan-Chang constitutive model. According to Duncan-Chang model, the material properties used in the next step need to be calculated with the current stress state.

Simulation of the confined compression test was conducted based on the Duncan-Chang constitutive model in Section 3.2. The inner diameter and height of the thin wall bucket are 476 mm and 500 mm respectively. Axisymmetric model was adopted, and a forced displacement was applied on upper boundary of model, as shown in Fig. 7. Because the stress of garbage is uniform everywhere in the whole model, the garbage can simply be set as one material instead of extracting stress from each element, recalculating its elastic modulus, Poisson's ratio and updating material properties. Therefore, simulation of the confined compression test becomes very simple at this time.

4.2. Analysis results

Analysis terminated due to element excessive distortion, and the final result is shown in Fig. 8, in which the maximum deformation only reached 181 mm. The average pressure curve with the forced displacement of the garbage is shown in Fig. 9. Meanwhile, the average pressure curve with the forced displacement of five tests of the fourth batch is shown in Fig. 9. As shown in the figure, the resistance of the garbage was weak at the early compression stage, and after that, the resistance has sharply increased. The elastic modulus of the garbage changed with average pressure, as shown in Fig. 10.

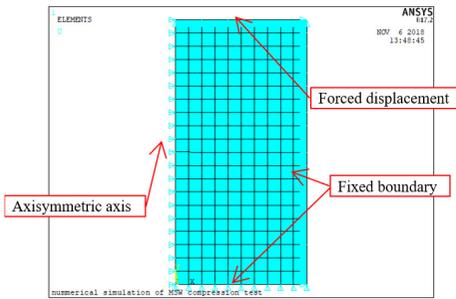


Fig. 7. Test model of waste compression

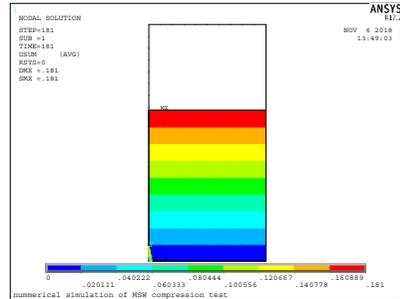


Fig. 8. Deformation of last step

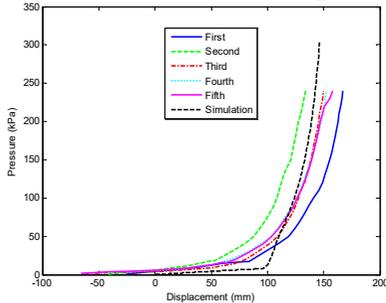


Fig. 9. The average pressure along the displacement curve of five tests of the fourth batch and simulation

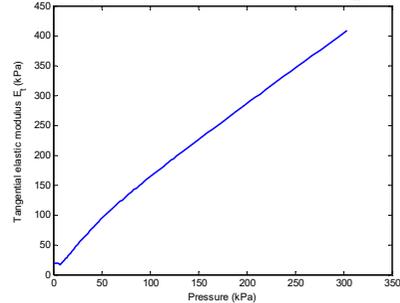


Fig. 10. The elastic modulus of the garbage changes with pressure

Firstly, geometric nonlinearity and contact nonlinearity were involved. Secondly, it is necessary to extract the principal stress of each element after each loadstep and recalculate and update the elastic modulus and Poisson's ratio according to the Duncan-Chang model. Thirdly, the garbage itself has a large deformation, and it may lead to element malformation and even negative volume, which results in the termination of the calculation. Generally, it is difficult to simulate

the whole garbage compression process according to the Duncan-Chang model.

5. Conclusions

In this paper, as the working objects of compression garbage trucks, the mechanical properties of fresh MSW were studied. A special test device combining the direct shear test with the confined compression test was designed, manufactured and assembled to conduct test about the fresh MSW. Detailed test data was obtained with direct shear test and confined compression test. And the Duncan-Chang constitutive model parameters by summarizing and organizing test data. Then the Duncan-Chang constitutive model parameters were used to simulate the confined compression test. The correctness of the parameters of the Duncan-Chang constitutive model of fresh MSW was verified, which provided a basis for the simulation and structure optimization of the garbage compression process of the compression garbage trucks.

References

- [1] **Zhang Bingyin, Jie Yuxin** Strength and deformation characteristics of waste soil. Engineering Mechanics, Vol. 23, Issue 2, 2006, p. 14-22, (in Chinese).
- [2] **Qian Xue De, Guo Zhi-Ping** Engineering properties of municipal solid waste. Chinese Journal of Geotechnical Engineering, Vol. 20, Issue 5, 1998, p. 4-9, (in Chinese).
- [3] **Sun Xiuli, Kong Xianjing, Zou Degao, et al.** Stress-strain model of municipal solid waste. Chinese Journal of Geotechnical Engineering, Vol. 30, Issue 5, 2008, p. 726-731, (in Chinese).
- [4] **Zhen-Ying Z., Li-Jun Y., Da-Zhi Wu** Experimental study of compression and direct shear combined test of fresh municipal solid waste. Rock and Soil Mechanics, Vol. 35, Issue 11, 2014, p. 3049-3055, (in Chinese).
- [5] **Zhen-Ying Z.** Study on Compressibility and Settlement of Landfill for Municipal Solid Waste. Zhejiang University, 2005, (in Chinese).
- [6] **Xuan P., Hua-Ping T.** Finite element analysis of rear-loaded garbage compressing cart based on Duncan-Chang constitutive model. Mechanical Research and Application, Vol. 3, 2015, p. 14-16, (in Chinese).
- [7] **Zhong M. Q., Xiao H. B., Huang Q., et al.** The optimization analysis of the lifting structure of the buried garbage compression station. Applied Mechanics and Materials, Vol. 364, 2013, p. 76-80.
- [8] **Qian Jiahuan, Yin Zongze** Geotechnical Principles and Calculations. China Water Resources and Hydropower Press, Beijing, 2000, (in Chinese).
- [9] **Wang X., Liu Z., Cui W.** Implementation of Duncan-Chang model in ANSYS and the inversion of its parameters. Proceedings of the 2nd International Conference on Modelling and Simulation, Vol. 7, 2009, p. 65-71.
- [10] **Guo P., Li W. C.** Development and implementation of Duncan-Chang constitutive model in GeoStudio2007. Procedia Engineering, Vol. 2, Issue 1, 2011, p. 395-402.
- [11] **Feng Shijin** Static and Dynamic Strength Characteristics of Municipal Solid Waste and Stability Analysis of Landfill. Zhejiang University, 2005, (in Chinese).