The impact of the passenger train speed on the comfort of humans in a building close to the railway

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Abstract. The article presents the impact of the speed of a passenger train on the comfort of humans in the building. Kinematic excitations were obtained from field tests and used in numerical calculations. Numerical calculations were made on the spatial FEA model of the residential building. The WODL ratio prediction curve was determined depending on the train speed.

Keywords: railway, vibrations, HST, human comfort, FEA model.

1. Introduction

The development of the railway line is associated with reducing the travel time between cities. Due to restrictions on the possibility of extending the railway line (shortening the section in terms of length), the easiest way is to increase the crossing speeds. Any investment related to a change in the operating conditions of a railway line requires the preparation of previous analyzes regarding the impact of the proposed change on the environment. In particular, this concerns the impact of railway modernization on neighboring buildings. The most important issue is the impact of vibrations on people in the building. In the world literature and country standards, the impact of vibrations on people is analyzed using various methods [1-7]. The Polish standard [8] specifies the procedure for evaluation the impact of vibrations on people in such cases. The following article presents the analysis of the impact of vibrations on people from the passage of a passenger train (electric integrated traction train) with different speeds on one of the main railway lines in Poland. The simulation works presented in the following article were preceded by field tests during which the vibrations of foundations of a residential building made in traditional brick technology were determined. The recorded accelerations were used as kinematic excitations in the analysis of the 3D FEM calculation model.

2. Field tests

In order to identify the impact of vibration velocity on the reception of vibrations by people in the building, 15 kinematic excitations were selected. All registrations were made on one measurement day in specific ground conditions on the foundation wall of a single-family building located approximately 40 m from the railway line. The calculations were carried out for crossing speeds 40, 80, 120, 160, 200, 230 and 250 km/h. At the present the train speed at the line is limited to 200 km/h. It is still much lower than in other countries, where railway is more developed. In China for example the influence of high speed trains (HST) for ground borne vibrations where examine for speed up to 410 km/h [9]. In Poland the next step in increasing the train speed for passenger trains is 250 km/h. The analyzed passenger train is presented in Fig. 1. It is an electric integrated traction train – code name Pendolino. Fig. 2 presents selected record of the vibration accelerations of the foundation at the speed of 250 km/h. Fifteen selected crossings of the train were analyzed. The assembly method of the sensors on the building’s foundation is presented in Fig. 3. All three components of ground vibration acceleration for all the analyzed velocities were used as a kinematic excitation in the 3D FEM model. More detailed description of the field tests is presented in papers [10, 11].
3. FEM model

A 3D calculation model based on the principles of Finite Element Method (FEM) was adopted (comp. Fig. 4). It is a typical residential building with a traditional construction. Structural elements such as beams and columns were modeled with beam finite elements (a two-node finite element with 6 degrees of freedom in the node), and surface elements such as walls and ceilings with shell elements (a four-node or three-node finite element with 6 degrees of freedom in the
node). The partition walls in the calculation model were treated as a substitute surface load. In the model, due to very good ground conditions, full constraint was assumed in the foundation level (\(T_x = T_y = T_z = R_x = R_y = R_z = 0\)). Fig. 4 the visualization of the building's calculation model.

\[\text{Fig. 3. Acceleration sensors mounted on the foundation of the building}\]

\[\text{Fig. 4. 3D FEA model and it's pose relative to the railway line}\]

For the entire structure, global damping with a critical fractional damping 5 % was assumed. This corresponds to buildings with a traditional brick construction. In the calculations, dead loads and 40 % of live loads were assumed. The calculations were made using the direct integration method with time step \(\Delta t = 0.000976 \, \text{s}\), which corresponds to 1024 Hz sampling. Kinematic loads were assumed in the form of recorded accelerations applied at the base of the model as a uniform excitation (comp. Fig. 2 as an example).

4. Results

Due to the structural layout and span length of monolithic ceilings in the building, the impact of vibrations on people was examined, in particular at the points specified in Fig. 5. The control points used in Fig. 5 were also used in the presentation of results. The results are presented in the form of bars on the graphs. The bars represent the RMS acceleration in one-third octave band. The lines at the graphs represents the thresholds of the comfort according to polish code [8]. The results are also presented as the WODL ratio. The WODL ratio (in English, the human vibration perceptivity ratio) [8], is the measure of vibration perception by people. It is the maximum ratio of the acceleration RMS value obtained from the analysis to the acceleration RMS value equivalent to the threshold for the perception of vibration by humans (in the same 1/3 octave band) chosen from each 1/3 octave band:
\[ WODL = \max \left( \frac{a_{RMS}}{a_z} \right), \]  

where: \( a_{RMS} \) – acceleration RMS value obtained from analysis in 1/3 octave band; \( a_z \) – acceleration RMS value equivalent to the threshold for the perception of vibration in a z-direction in the same 1/3 octave band as in \( a_{RMS} \).

The selected analysis result of the influence on human in the building is presented in Fig. 6, while results for all analyzed events are presented in the Table 1. The aggregate results for all the analyzed events are shown in Fig. 7. For the obtained results, the WODL ratio has been developed exponential lines of the trend. Trend lines have been developed in two variants: for speeds from 40 to 230 km/h and for speeds from 40-250 km/h. A good mapping of the trend to a speed up to 230 km/h was observed. The increase in the WODL index is has an exponential nature and it is possible to use it to predict WODL values at changes in the crossing speed of the analyzed train. At 250 km/h, a decrease in WODL ratio was observed. This is probably related to the shift in the phase of frequency excitation. In this case, analyzes are necessary for different types of buildings and different ground conditions.

**Table 1. Results of the analysis – WODL ratios**

<table>
<thead>
<tr>
<th>No.</th>
<th>Speed [km/h]</th>
<th>Central frequency [Hz]</th>
<th>WODL [-]</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>40</td>
<td>20</td>
<td>0.20</td>
</tr>
<tr>
<td>2</td>
<td>80</td>
<td>16</td>
<td>0.32</td>
</tr>
<tr>
<td>3</td>
<td>120</td>
<td>16</td>
<td>0.33</td>
</tr>
<tr>
<td>4</td>
<td>160</td>
<td>16</td>
<td>1.60</td>
</tr>
<tr>
<td>5</td>
<td>160</td>
<td>16</td>
<td>1.71</td>
</tr>
<tr>
<td>6</td>
<td>200</td>
<td>16</td>
<td>3.08</td>
</tr>
<tr>
<td>7</td>
<td>200</td>
<td>16</td>
<td>2.86</td>
</tr>
<tr>
<td>8</td>
<td>200</td>
<td>16</td>
<td>2.60</td>
</tr>
<tr>
<td>9</td>
<td>230</td>
<td>16</td>
<td>5.14</td>
</tr>
<tr>
<td>10</td>
<td>230</td>
<td>16</td>
<td>5.21</td>
</tr>
<tr>
<td>11</td>
<td>250</td>
<td>20</td>
<td>2.62</td>
</tr>
<tr>
<td>12</td>
<td>250</td>
<td>20</td>
<td>2.72</td>
</tr>
<tr>
<td>13</td>
<td>250</td>
<td>16</td>
<td>5.07</td>
</tr>
<tr>
<td>14</td>
<td>250</td>
<td>20</td>
<td>2.89</td>
</tr>
<tr>
<td>15</td>
<td>250</td>
<td>20</td>
<td>3.06</td>
</tr>
</tbody>
</table>
5. Conclusions

The performed tests and analyzes indicate that in the current speed limits, the impact of vibrations on people according the code [8] is satisfied. For higher speeds, the comfort threshold was exceeded in individual cases. There is no vibro-insulation in the track construction. In the case of raising the speed up to 250 km, it may be necessary to install vibro-insulation in the track in order to ensure the comfort for people in the buildings close to the railway line. The zones of influence of the railway lines on people in the buildings were already analyzed in the work [12]. The results presented in the above paper may be used for their development for future train speeds.

References


THE IMPACT OF THE PASSENGER TRAIN SPEED ON THE COMFORT OF HUMANS IN A BUILDING CLOSE TO THE RAILWAY.

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