

A new machinery diagnosis method based on complex bilateral spectrum

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Abstract. In view of the turbo molecular pump high-speed rotating parts, this paper presents a new machinery diagnosis method based on complex bilateral spectrum. At first, the vertical and horizontal vibration signals are directly combined into complex signals in time-domain; and then the complex bilateral spectrum is obtained by fast Fourier transform (FFT). Furthermore, the holospectrum, which can fast find machinery faults, can be obtained using the amplitude and phase at some special frequencies. At the same time, the equivalence of holospectrum technique and the proposed method is verified. Finally, a case study shows the effectiveness of the proposed method.

Keywords: complex number, bilateral spectrum, characteristic parameters, holospectrum.

1. Introduction

A turbomolecular pump uses the opposite movement between high-speed spinning moving blades and static blades, which drives gas molecules from higher vacuum zone to the lower zone. Afterwards, gas molecules are pumped into the air through the backing pump to create vacuum. So far, methods like FFT amplitude spectrum [1], Orbit Center of Shaft [2], Waterfall Plot [3] continue to be widely used in fault diagnosis of high-speed spinning part. However, the amplitude and phase in methods are separate, which is not straightforward and has a greater phase difference [4]. Since the late 1980's of last century, holospectrum [4] and Full Vector Spectrum have been continually put forward to handle the separation problem of single amplitude and phase. The core of the holospectrum technology is to conduct FFT transform [5] on signals along x and y directions in a bearing face of the rotor. Then the unilateral spectrum is used to integrate amplitude and phase of two directions thus the orbit of center shaft is obtained. The Full Vector Spectrum synthesizes signals along x and y direction into a single complex and then FFT transform is conducted. The unilateral spectrum along x and y direction are drawn and synthesized from the complex amplitude and phase spectrum, where the orbit of center shaft is obtained.

It can thus be seen that the holospectrum and full vector spectrum both use the unilateral spectrum of x and y . However, only the positive frequencies are synthesized, where the process is complicated and not straightforward. This paper presents a fault diagnosis technology based on complex bilateral spectrum analysis, where vibration signals are treated as complex and FFT transform is directly conducted. Thus fault parameters are directly obtained.

2. The principle of complex bilateral spectrum diagnosis

2.1. The kinetic model of rotor vibration [6]

In order to determine the position center o' of the disk when it rotates, the fixed coordinate system $Axys$ is used as a reference. The coordinate of o' is expressed as x and y . Suppose the center of the rotating axis goes through the disk center and it rotates at a constant angular speed of Ω . When the disk rotates normally, its spin axis is perpendicular. If a side shock is imposed, the flexural vibration of spin axis or side vibration of disk happens due to its resilience. The mass of

the disk is expressed as m . Its weight is the elastic restoring force F of the spin axis:

$$F = -kr, \tag{1}$$

where, k is the stiffness coefficient of the spin axis, $r = \infty$. Relative to the fixed coordinate system Axy , the differential motion equation of the disk is:

$$m\ddot{x} = F_x = -F \frac{x}{r} = -kx, \quad m\ddot{y} = F_y = -F \frac{y}{r} = -ky.$$

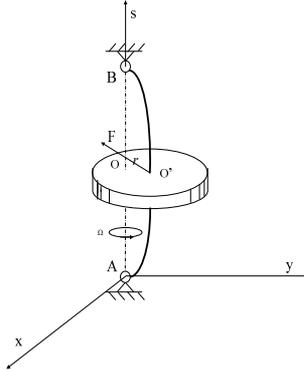


Fig. 1. Rotor model

Assume that:

$$\omega_n^2 = \frac{k}{m}, \tag{2}$$

$$\begin{cases} \ddot{x} + \omega_n^2 x = 0, \\ \ddot{y} + \omega_n^2 y = 0. \end{cases} \tag{3}$$

The solution to the equation is:

$$\begin{cases} x = X \cos(\omega_n t + a_x), \\ y = Y \sin(\omega_n t + a_y). \end{cases} \tag{4}$$

Suppose that:

$$z = x + iy (i = \sqrt{-1}).$$

The Eq. (3) becomes:

$$\ddot{z} + \omega_n^2 z = 0. \tag{5}$$

Its solution is:

$$z = B_1 e^{i\omega_n t} + B_2 e^{-i\omega_n t}, \tag{6}$$

where B_1 and B_2 both are complex, which are determined by the initial side shock. The first item is an anticlockwise motion of the radius $|B_1|$, in the same direction of the rotation angular speed Ω , which is called forward precession. The second item is a clockwise motion of the radius $|B_2|$, in the opposite direction of the angular speed Ω , which is called backward precession. Both

precessions synthesize the vortex motion of the disk center o' . Due to different initial conditions, following situations of disk center motion may occur:

- 1) $B_1 \neq 0, B_2 = 0$; The vortex motion is forward, where its orbit is a circle and the radius is $|B_1|$.
- 2) $B_1 = 0, B_2 \neq 0$; The vortex motion is backward, where its orbit is a circle and the radius is $|B_2|$.
- 3) $B_1 = B_2$; The orbit is a straight line and the point o' works as a simple harmonic vibration.
- 4) $B_1 \neq B_2$; The orbit is an oval. When $|B_1| > |B_2|$, o' vortex motion is forward. When, $|B_1| < |B_2|$, o' vortex motion is backward.

2.2. The principle of complex bilateral frequency

It can be seen from Eq. (6), that the orbit of shaft center can be uniquely determined by B_1, B_2 and $\pm\omega_n$, where $-\omega_n$ is the backward precession frequency. On the other side, B_1, B_2 and $\pm\omega_n$ can be easily determined when FFT transform is conducted on z . The correspondent amplitude spectrum and phase spectrum can be obtained when matched with B_1, B_2 and $\pm\omega_n$ (Fig. 2). Since ω_n has both positive and negative part, it is called “bilateral frequency”. The orbit of shaft center can be further obtained and the correspondent fault parameters can thus be obtained.

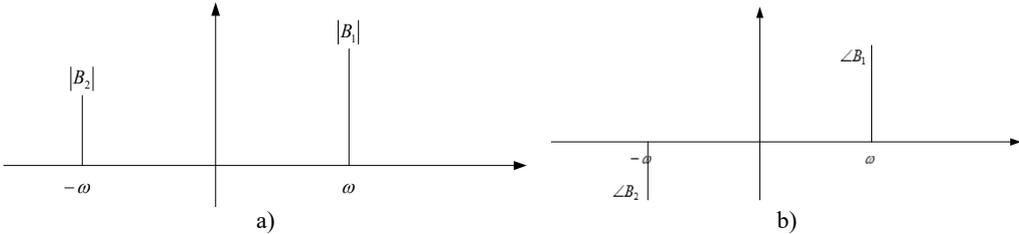


Fig. 2. a) Amplitude spectrum of z and b) phase spectrum of z

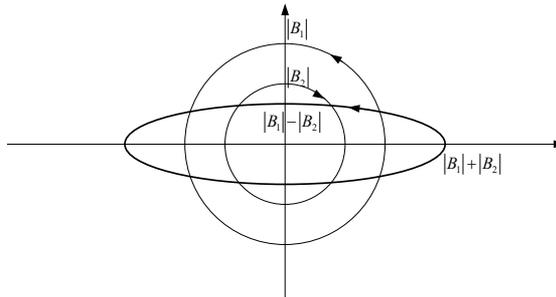


Fig. 3. Synthesizing diagram of shaft center orbit

3. The equivalence of complex bilateral spectrum and holospectrum

The holospectrum utilizes coefficients x, y in Eq. (4), and a_x, a_y to synthesize the orbit of shaft center. Complex vector spectrum uses x and y to synthesize complex z and to get expression like Eq. (6). The complex coefficient B_1 and B_2 synthesize the orbit of shaft center. Essentially, they are completely equivalent and the following proof is given.

Proof: Since, $\cos\omega t = (e^{i\omega t} + e^{-i\omega t})/2$ the following can be obtained when $\sin\omega t = i(e^{-i\omega t} - e^{i\omega t})/2$ is taken into Eqs. (4) and (6), then $z = B_1 e^{i\omega t} + B_2 e^{-i\omega t}$ is obtained. Where:

$$B_1 = \frac{X^{ia_x} + Y e^{ia_y}}{2}, \quad B_2 = \frac{X^{-ia_x} - Y e^{-ia_y}}{2}. \tag{7}$$

It can be seen that Eqs. (7) and (4) are equivalent. That is to say, the bilateral spectrum of z and the unilateral spectrum of x and y are equivalent in synthesizing the shaft center orbit.

4. Experiment verification

The experiment chooses the fault data of a molecule pump running at the speed of 10000 rpm (166.028 Hz) to analyze, where sampling frequency is 2560 Hz and data length is 1024. Fig. 4 is the time domain data sampled by the equipment developed by Beijing Air Intelligent Control Monitor Technology Institute. Fig. 5 is time domain signal of x and y in MATLAB. Fig. 6 is the unilateral spectrum of x and y signals and the bilateral spectrum of $x + iy$. The fault of x and y signal is unable to determine in the time domain. So this signal needs processing, mainly concerning orbit of particular frequencies like $1X$, $2X$, $3X$, $4X$ and correspondent parameters are extracted.

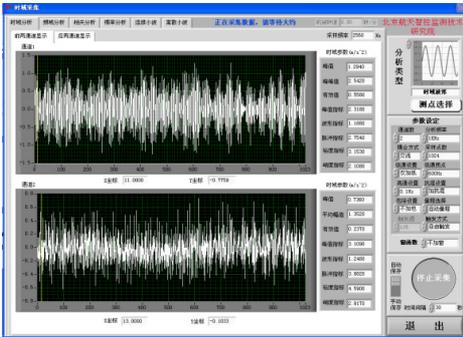


Fig. 4. Time domain data sampled

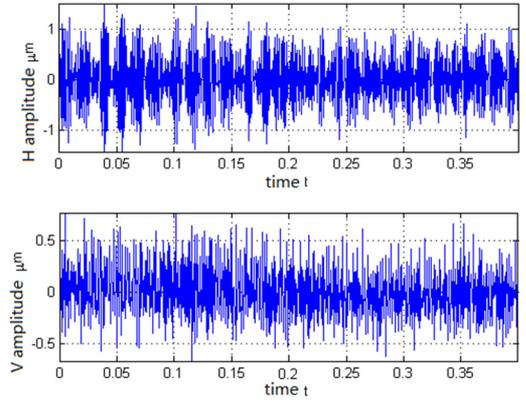


Fig. 5. Time domain signals of x and y axis

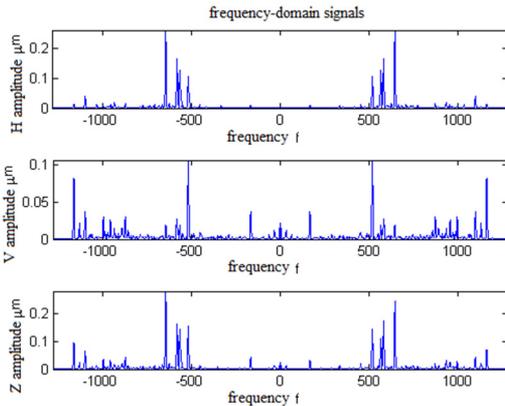


Fig. 6. Unilateral spectrum of x and y direction and bilateral spectrum of $x + iy$

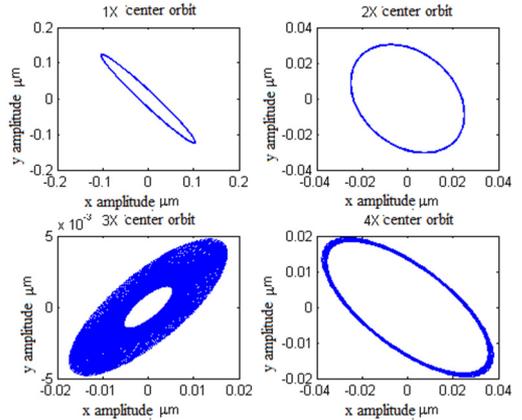


Fig. 7. Correspondent holospectrum

FFT transform is conducted according to the complex synthesized by x and y and dual frequency is obtained. It can be seen that the eccentricity of the quadruple frequency is greater and the rotor misalignment fault exists.

Meanwhile, the holospectrum [7] is used to analyze the fault, as the following shows: firstly, FFT transform is conducted on x and y signal to get unilateral spectrum. Then the major axis radius and minor axis radius are calculated. Afterwards, the forward and backward precession

circle radius is obtained and the oval is synthesized. It is compared with the method in this paper, shown in Table 1.

Table 1. Comparison of this method and holospectrum

	FFT times	Precession circle radius	Oval turning direction determination	Oval synthesize
Complex spectrum	One	Read directly	Determine directly	Directly synthesize
Holospectrum	Two	Indirectly calculate	Indirectly determine	Directly synthesize

5. Conclusions

This paper puts forwards a fault analysis method based on complex bilateral spectrum. The method is not only essentially equivalent to holospectrum but also more direct and effective than it. FFT transform and spectrum correction are conducted for only one time without separate analysis of x and y direction. Besides, backward and forward precession parameters can be directly seen from bilateral spectrum, which directly reflects the holospectrum technology of Bently company. It is thus clear that the holospectrum technology, vector spectrum are only part of this method.

References

- [1] **Wang Z. G., Zhu S. R.** The FFT-FS spectrum refining technology and its application in machinery diagnosis. Journal of Wuhan University of Science and Technology: Science Edition, Vol. 1, Issue 23, 2000, p. 44-46.
- [2] **Cheng H., Du L. S.** The shaft center orbit fault diagnosis of rotating machinery. Journal of Taiyuan University of Technology, Vol. 5, Issue 34, 2003, p. 1-2.
- [3] **Jiang H., Wang Y. Z.** Online condition monitoring and fault diagnosis system development of rotating machinery. Oil Field Machinery, Vol. 3, Issue 34, 2005, p. 68-70.
- [4] **Qu L. S.** Holographic Diagnosis Principle of Machinery Fault. Science Press, 2007.
- [5] **Burrus C., Parks T. W.** DFT/FFT and Convolution Algorithms: Theory and Implementation. Science Press, 2007.
- [6] **Zhong Y. E., He Y. Z., Wang Z. C.** Rotor Dynamics. Tsinghua University Press, 1987.
- [7] **Bently E., Hatch T., Grissom D. C. B.** Fundamentals of Rotating Machinery Diagnostics. Bently Pressurized Bearing Press, 2002.